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#### **EAE Seismic Bracing System Solutions**

It is utmost important to seismically restrain mechanical and electrical distribution systems in a building, which are defined as non-structural components. These distribution systems should be protected via seismic bracing installations that are attached to structural components, against risks of breaking and failure.

EAE is a manufacturing company, specialized on busbar distribution systems, cable trays and lightening group products. EAE has been supplying products to industrial facilities, residential buildings, shopping malls, airports, hospitals, car manufacturers and similar facilities for forty years. EAE, also produces support installation components for these systems. However in the local market, lack of seismic support systems with additional calculations, testing and the production of proper seismic bracings were an important issue.

EAE, with wide range of products and long years of experience, has taken an important step with seismic bracing systems as an addition to its product groups in order to eliminate this inadequacy.

The seismic bracing systems are designed according to international standards. The general approach was, to design a cost efficient system that can be used in multiple ways, easily installed and cut labor costs.

In hospitals, education facilities, high risers, residences, shopping malls, power plants, automotive, steel and glass producing facilities, oil&gas facilities, which are located at seismic risk areas, seismic bracings with calculated load resistances have become a necessity for life safety and operational persistency.

With EAE seismic bracing products you can find solutions for electrical and mechanical distribution service seismic resilience on your building.

#### ▶▶ 1. Fundamental Earthquake Knowledge



An earthquake can be described basically as shaking of ground.

There are three types of natural earthquakes:

#### 1. Collapse Earthquakes

Earthquakes with limited area of effect, occurred by collapse of underground gaps such as caves and mines.

#### 2. Volcanic Earthquakes

Earthquakes occurring as a result of volcanic activities.

#### 3. Tectonic Earthquakes

It is the most commonly felt earthquake type. It occurs by the movement of plates, which generates earth's crust.

#### Plate Theory

This is the theory, which was put forward to understand and study the nature of earthquakes, largely accepted as early states and in the epicenter of earthquake studies. According to theory, earth's crustal mass stand on plates and those plates are ever moving. From past to present continents are formed by the movement of these plates and become distant to each other.



PERMIAN 250 million years ago



TRIASSIC 200 million years ago



JURASSIC 145 million years ago

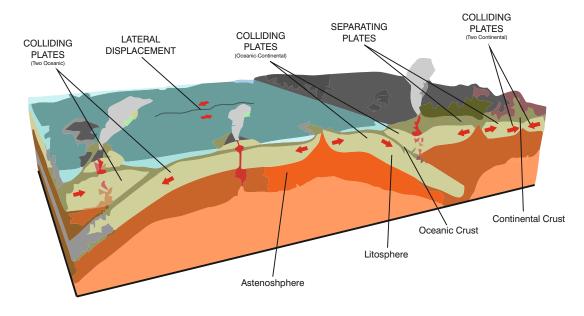


CRETACEOUS 65 million years ago



PRESENT DAY

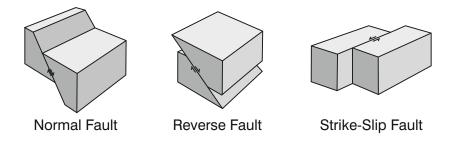
The inner areas of plates are relatively stable. But on the edges, where plates collide, they create fault lines and leads to major earthquakes.



#### ▶▶ 1.Fundamental Earthquake Knowledge

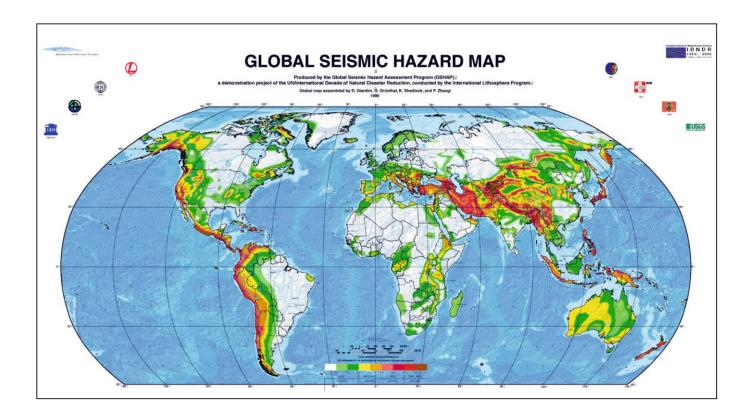


Figure 1.1 shows three main fault types.



**Figure 1.1 Three Main Fault Types** 

Regions with intense seismic activities are located around those fault lines, where plates are colliding. Global seismic hazard map can be seen below.



#### ▶▶ 2. Earthquake Safety of Distribution Systems



#### **Earthquake Hazard of Distribution Systems**

Researches on the subject shows that, up to 80% of the damage and loss are because of the fires following the earthquake. The functionality of sprinkler systems and electrical&mechanical distribution systems during and after an earthquake takes great importance in the present modern buildings. To mitigate life and financial loss from dysfunctionality of the distribution systems, proper seismic bracing is the most effective method.



Figure 2.1a Earthquake Hazard of Electrical Conduits (Images from Federal Emergency management Agency Website, www.fema.gov)



Figure 2.1b Earthquake Hazard of Electrical Transformers (Images from Federal Emergency management Agency Website, www.fema.gov)

#### ▶▶ 2. Earthquake Safety of Distribution Systems



#### Calculation of Seismic Loads

Any seismic force affecting a distribution system component in any level of the building is the result of the earthquake acceleration. Seismic force can be calculated according to principal physics equitation F=m.a (Figure 2.2). Seismic acceleration should be determined in order to calculate effecting force. Earthquake acceleration can be determined by various international and local codes.

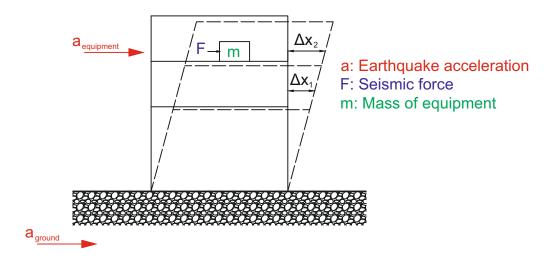


Figure 2.2 Earthquake Acceleration and Earthquake Load

Most accepted building code for seismic applications since 2011 is IBC® 2012 (International Building Code) which is governed by ICC® (International Code Council). According to IBC® 2012, where needed, seismic design force can be calculated by the equitation below:

$$F_{p} = \frac{0.4a_{p}S_{DS}W_{p}}{\frac{R_{p}}{I_{p}}} \left(1 + 2\frac{z}{h}\right) \quad (1)$$

Values shown in seismic design force (F<sub>□</sub>) described below:

**a**<sub>p</sub>: Component amplification factor.

 $S_{DS}$ : Short period spectral acceleration.

 $W_p$ : Component operating weight.

**z**: Height in structure of point of attachment of component with respect to the base.

**h**: Average roof height of structure with respect to the base.

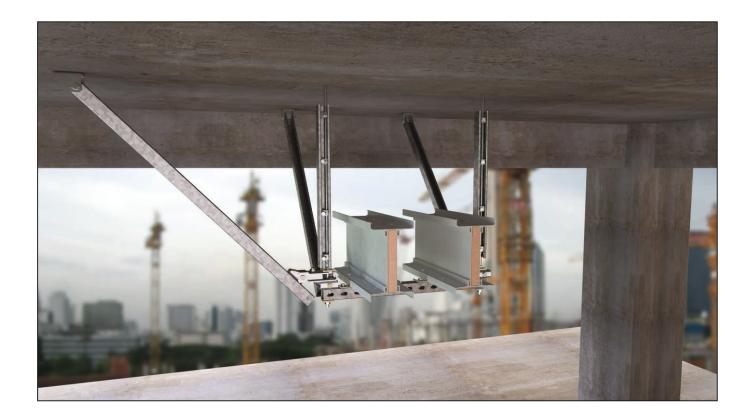
 $\mathbf{R}_{p}$ : Component response modification factor.

 $I_p$ : Component importance factor.

#### ▶▶2. Earthquake Safety of Distribution Systems



As seen in eq. 1, short period spectral acceleration ( $S_{ps}$ ) should be defined by designer in order to calculate seismic design force ( $F_p$ ). Additionally because of short period spectral acceleration ( $S_{ps}$ ) value contains certain constants for soil condition, it can be possible to calculate project specific earthquake loads. Likewise, component importance factor ( $I_p$ ) can be determined by the requirements of project and/or demand of the project owner.





#### ▶▶3. Seismic Bracing Applications



#### **Suspended Equipments**

To protect an equipment suspended via threaded rods or steel elements against seismic forces, equipment sould be restrained with seismic braces. The brace should satisfy seismic design load requirements. Seismic brace installation usually done by fixing the brace with  $45^{\circ}\pm10^{\circ}$  angle both horizontal and vertical (Figure 3.1). The essential informations should be provided with supporting installation drawings and selection sheets as proof of brace meets the design load criteria.

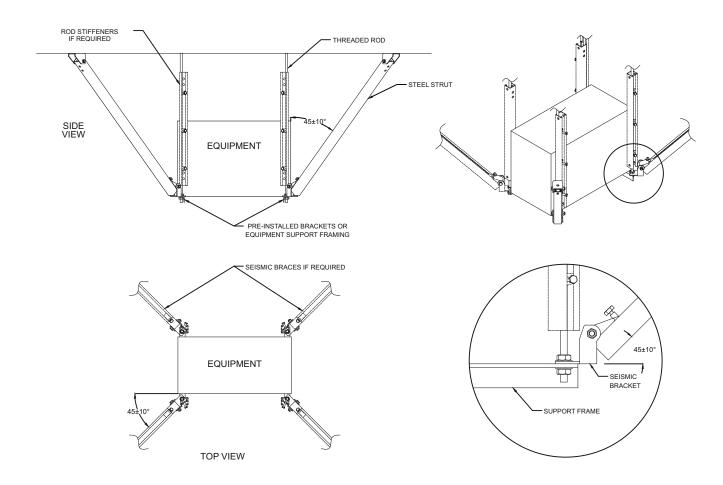


Figure 3.1 Seismic Bracing of Suspended Equipments

#### ▶▶3. Seismic Bracing Applications



#### **Distribution Systems**

One of the critical non-structural seismic protection topic is electrical distibution systems. Main reason behind this is the variable components that are used to support bus ducts, conduits and cable trays. They can be suspended, wall fixed or floor supported. The crucial point is that every system in buildings, including essential fire pumps and other emergency systems, are powered by the electrical distribution systems. Generally suspended disribution systems are the most vulnerable non-structural components against seismic forces. Especially emergency systems like sprinkler pipes are fragile because of high pressure liquid inside. One crack on main pipe can turn into a system failure. Protection of the suspended distribution systems, depending on project, are done by creating layouts of lateral and longitudinal bracing points. For the first step of determining seismic fixing points, lines should be given numbers (Figure 3.2). Then lateral braces should be provided on both end of the each line.

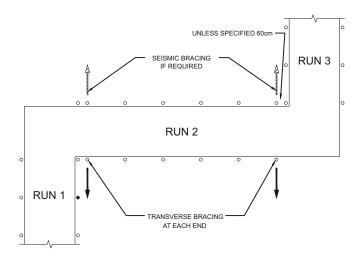


Figure 3.2 Layout of Lateral Braces on Both End

Although it can differ from specification to specification, generally maximum allowed spacing of lateral brace is 9m (30 ft) for HVAC ducts, busbar and cable trays, 12m (40 ft) for pipes and conduits. Again it can be generalized to 18m (60 ft) maximum allowed space between two longitudinal brace for HVAC ductwork, busbar and cable trays, 24m (80 ft) for pipes and conduits. If the spacing between two lateral brace at both end of the line is greater than allowed, more seismic braces should be added in order to meet required maximum brace spacing (Figure 3.4).

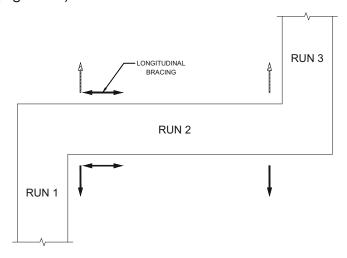


Figure 3.3 Layout of Longitudinal Brace for Each Line

#### ▶▶3. Seismic Bracing Applications



Each line should have at least one longitudinal brace (Figure 3.3). If the length of the line is greater than maximum longitudinal brace span, more longitudinal braces should be added until the spacing bettween two longitudinal brace meets requirements (Figure 3.4).

Additionally, for being cost effective, the junction points of lines should be braced both lateral and longitudinal (Figure 3.4). In doing so, lateral brace works as longitudinal brace of the other line. Further cost decrease can be achieved by making 45° angular bracing designs, in order to make brace restrain both lateral and longitudinal loads (Figure 3.4).

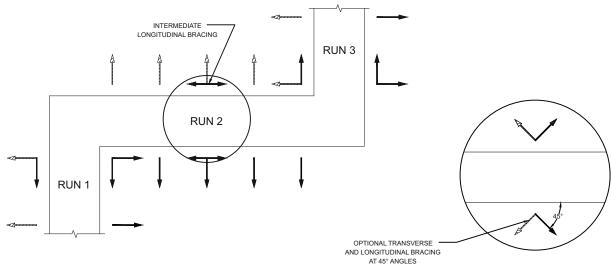


Figure 3.4 Angular Fourway Brace

Seismic fixings on distribution systems can be composed of steel struts or cables. But cables are tension only systems. Therefor two components are needed instead of one steel strut.

In cases, where multiple pipelines are suspended via trapeze supports, trapeze must be braced. Essential point on trapeze supports are the necessity of pipes being properly fixed at trapeze. Fixing have to meet seismic load requirements. In order to do this, U-straps or U-Bolts should be used (Figure 3.5). Classical one-point fix pipe clamps are usually inadequate because of the consisting moment on the fix point during a seismic event.

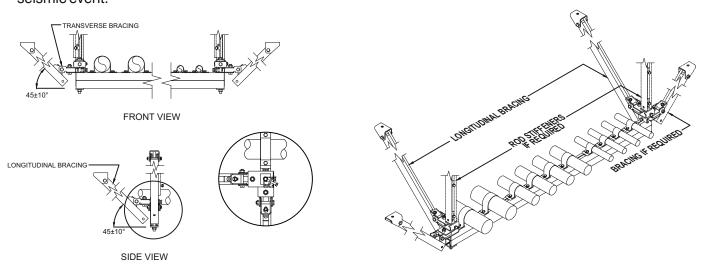


Figure 3.5 Multiple Pipe Fixings on Trapeze Assembly

#### ▶▶3. Seismic Bracing Applications



#### **Cable Trays and Other Systems**

Suspended cable trays, conduits, busbars and HVAC ductworks, should also be braced with steel struts or cables (Figure 3.6). If it is wall supported or floor supported, it can be unnecessary to restrain it with additional seismic bracing, provided that structural component to be fixed is secure.

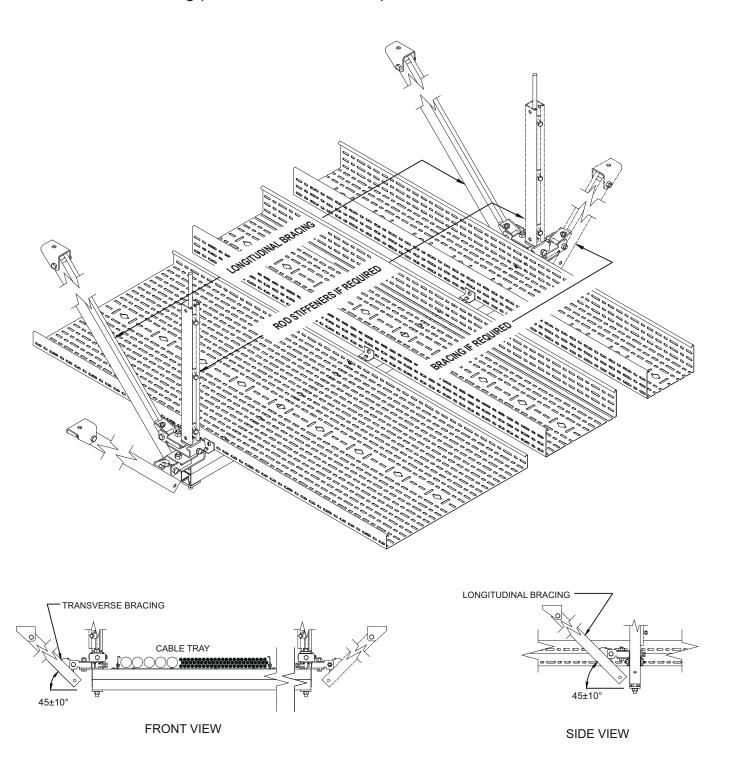


Figure 3.6 Seismic Bracing of Cable Trays

#### ▶▶3. Seismic Bracing Applications



#### **Application Examples**

All distribution systems can be practically protected by using rigid (steel strut) seismic bracings (Figure 3.7-10).



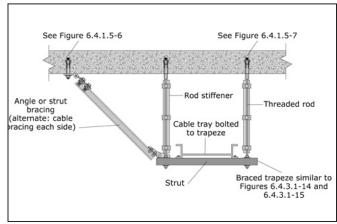






Figure 3.7, 3.8, 3.9, 3.10 Rigid Seismic Bracing (Steel Strut) Applications on Cable Trays and Conduits (Images from Federal Emergency Management Agency Website, www.fema.gov)



#### ▶▶3. Seismic Bracing Applications



#### Seismic Bracing Layout - General Procedure

The following pages outline the steps to take when laying out the placement of seismic bracing for a mechanical or electrical system. Refer to the appropriate codes and standarts for additional information and requirements.

#### STEP 1

Begin by seperating the system to be braced into individual runs of pipe, conduit or duct. A run is defined as a section between two changes in direction. A single run may have an offset or several offsets. These minor directional changes may be ignored if the overall distance perpendicular to the run does not exceed 1/16 of the maximum allowable transverse spacing.

**Example:** I you have a run of that does not exceed 9m (30') and your maximum allowable transverse spacing is 9m (30') you can have an offset in this run up to 9m/16 = 0.57m (30'/16 = 1'-10").

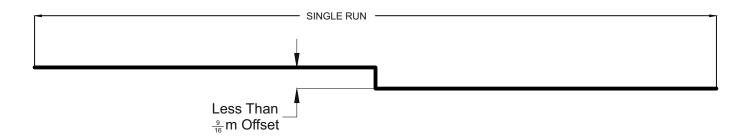


Figure 3.11 Run with Single Offset

**Example:** A run with several offsets can be treated the same way. As in the example above, assume that this run is 12m (30') long. As long as the total offset is no more than 0.57m (1'-10") long it can be braced as one run.

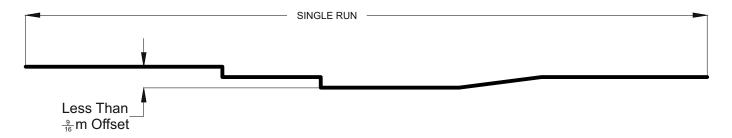


Figure 3.12 Run with Several Offsets



#### ▶▶3. Seismic Bracing Applications



#### STEP 2

Each run must be braced in the transverse direction at each end of the run.

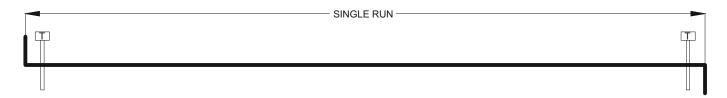


Figure 3.13 Transverse Bracing at Both Ends of the Run

If the distance between the two transverse braces exceeds the maximum allowable spacing, add transverse braces as needed.

**Example:** If you have a run to brace that is 18m (60') long, first place transverse braces at each end. One more brace is required along this run so that the maximum spacing of 9m (30') is not exceeded.

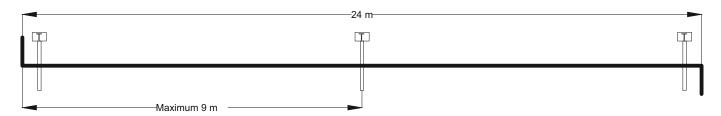


Figure 3.14 Additional Transverse Brace

#### STEP 3

Each run must have at least one longitudinal brace. If the maximum allowable longitudinal spacing is exceeded then add longitudinal braces to meet the spacing requirement.

**Example:** If you have a run that is 27m (90') long, first place one longitudinal brace along the run, then place additional longitudinal braces so the maximum allowable spacing is not exceeded.

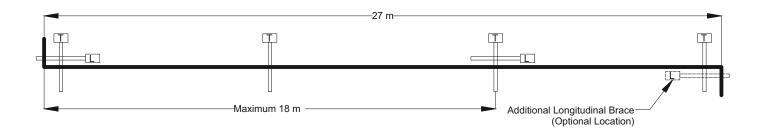


Figure 3.15 Longitudinal Braces

#### ▶▶3. Seismic Bracing Applications



To increase the efficiency of your bracing, a "DUAL USE" transverse brace within 60 cm (24") of a 90 degree elbow on an adjacent run can be used as longitudinal brace for the run being considered.

**Example:** If you have a run that is 27m (90') long, an adjacent "DUAL USE" transverse brace acts as a longitudinal brace for this run. The spacing is half the distance to the next longitudinal brace plus half the distance to the adjacent transverse brace (18/2+9/2=13,5m)

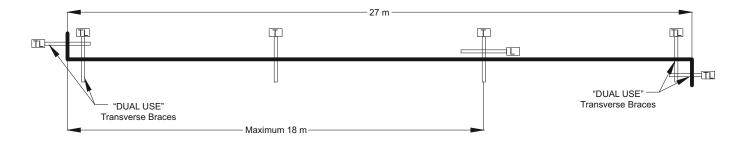


Figure 3.16 "DUAL USE" Seismic Braces

#### STEP 4

In some cases several short runs may occur in close proximity. By following the preceeding guidelines each run should have longitudinal and transverse bracing. Transverse bracing may be used as longitudinal bracing and vice versa on runs adjacent to each other as long as the total lenght of pipe tributary to the brace does not exceed the maximum allowable spacing. In cases where it does, additional braces are required.

**Example:** If the offsets are greater than the allowable length, pipe sections cannot be treated as one run. However, the number of braces can be minimized by using transverse braces as longitudinal braces and vice versa.

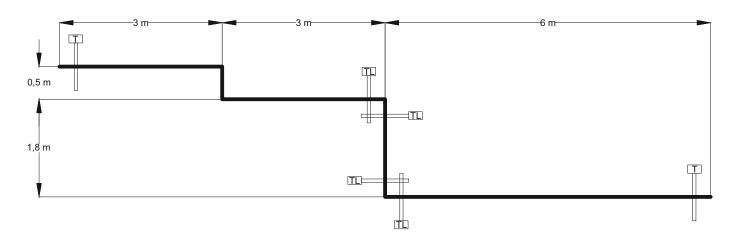


Figure 3.17 Number of Brace Decrease Applying "DUAL USE" Braces

#### ▶▶3. Seismic Brace Applications



#### STEP 5

At vertical pipe drop to mechanical equipment, where pipe is connected to the equipment using a flexible connection, provide transverse bracing before the vertical drop. The total length from the transverse brace to the vertical drop should not be more than the allowable offset previously determined. Provide transverse bracing at the floor after the vertical drop if the total length of the pipe from the transverse brace before the vertical drop to the flexible connection is greater than ½ of the maximum transverse brace spacing.

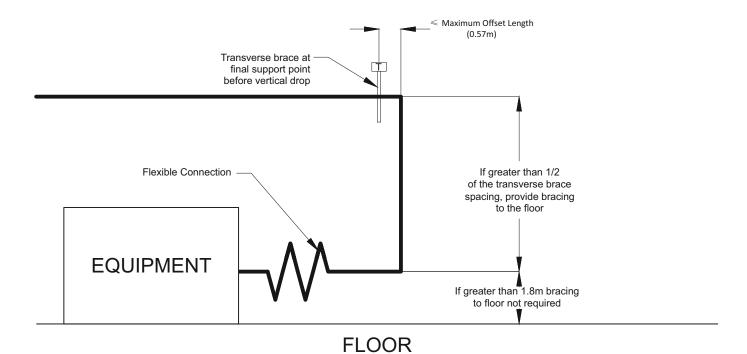
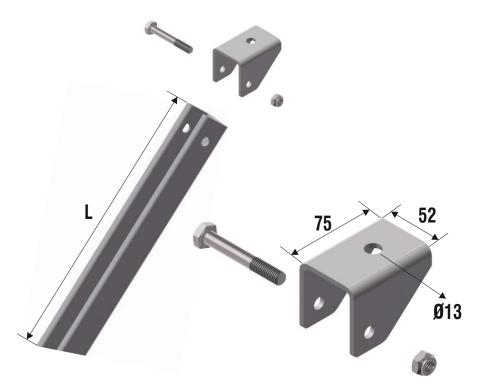


Figure 3.18 Seismic Bracing on Equipment Connections

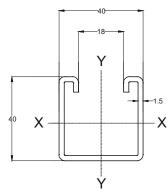
#### ▶▶4. Products



Description	L (mm)	T (mm)	Order Unit	Weight (kg/set)	Order Code
BR 401 Seismic Brace Section L: 500	500	1,5	Set	1,530	3046473
BR 401 Seismic Brace Section L: 600	600	1,5	Set	1,767	3046474
BR 401 Seismic Brace Section L: 700	700	1,5	Set	2,003	3046475
BR 401 Seismic Brace Section L: 800	800	1,5	Set	2,240	3046476
BR 401 Seismic Brace Section L: 900	900	1,5	Set	2,477	3046477
BR 401 Seismic Brace Section L: 1000	1000	1,5	Set	2,713	3046478
BR 401 Seismic Brace Section L: 1100	1100	1,5	Set	2,950	3046479
BR 401 Seismic Brace Section L: 1200	1200	1,5	Set	3,186	3046480
BR 401 Seismic Brace Section L: 1300	1300	1,5	Set	3,425	3046481
BR 401 Seismic Brace Section L: 1400	1400	1,5	Set	3,660	3046482
BR 401 Seismic Brace Section L: 1500	1500	1,5	Set	3,896	3046483
BR 401 Seismic Brace Section L: 2000	2000	1,5	Set	5,079	3046484
BR 401 Seismic Brace Section L: 2500	2500	1,5	Set	6,262	3046485
BR 401 Seismic Brace Section L: 3000	3000	1,5	Set	7,445	3046486
BR 401 Seismic Brace Section L: 3500	3500	1,5	Set	8,628	3046487
BR 401 Seismic Brace Section L: 4000	4000	1,5	Set	9,811	3046488
BR 401 Seismic Brace Section L: 5000	5000	1,5	Set	12,177	3046490
BR 401 Seismic Brace Section L: 6000	6000	1,5	Set	14,543	3046492
BR 401 Seismic Brace Section L: 7000	7000	1,5	Set	16,943	3046489
BR 401 Seismic Brace Section L: 8000	8000	1,5	Set	19,267	3046491



## BR401



#### **Assembly Includes**

- 1,5 mm 40x40 Binrak steel channel Hot-dip galvanize finish
- Seismic brace ceiling attachment special zinc finish
- M10X70 bolt
- M10 Fiber nut

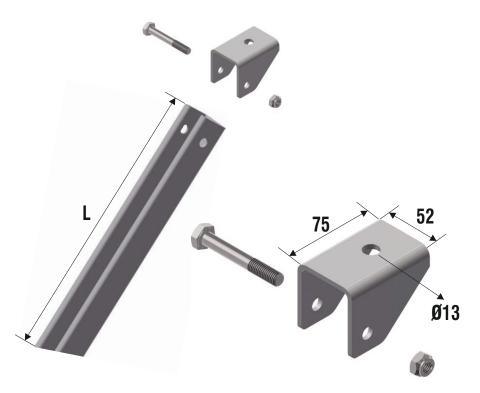
#### Please indicate order code in your orders.

- $\blacksquare$  4000 mm and over 4000 mm orders should be attached
- $\blacksquare$  Material weights are approximate values, it can variate  $\pm 10\%$ .
- Please call us for non-standard components.

#### ▶▶4. Products



Description	L (mm)	T (mm)	Order Unit	Weight (kg/set)	Order Code
BR 461 Seismic Brace Section L: 500	500	2,5	Set	1,825	3046493
BR 461 Seismic Brace Section L: 600	600	2,5	Set	2,121	3046494
BR 461 Seismic Brace Section L: 700	700	2,5	Set	2,417	3046495
BR 461 Seismic Brace Section L: 800	800	2,5	Set	2,712	3046496
BR 461 Seismic Brace Section L: 900	900	2,5	Set	3,008	3046497
BR 461 Seismic Brace Section L: 1000	1000	2,5	Set	3,304	3046498
BR 461 Seismic Brace Section L: 1100	1100	2,5	Set	3,600	3046499
BR 461 Seismic Brace Section L: 1200	1200	2,5	Set	3,895	3046500
BR 461 Seismic Brace Section L: 1300	1300	2,5	Set	4,191	3046501
BR 461 Seismic Brace Section L: 1400	1400	2,5	Set	4,487	3046502
BR 461 Seismic Brace Section L: 1500	1500	2,5	Set	4,783	3046503
BR 461 Seismic Brace Section L: 2000	2000	2,5	Set	6,261	3046504
BR 461 Seismic Brace Section L: 2500	2500	2,5	Set	7,740	3046505
BR 461 Seismic Brace Section L: 3000	3000	2,5	Set	9,219	3046506
BR 461 Seismic Brace Section L: 3500	3500	2,5	Set	10,698	3046507
BR 461 Seismic Brace Section L: 4000	4000	2,5	Set	12,176	3046508
BR 461 Seismic Brace Section L: 5000	5000	2,5	Set	13,655	3046509
BR 461 Seismic Brace Section L: 6000	6000	2,5	Set	15,134	3046510
BR 461 Seismic Brace Section L: 7000	7000	2,5	Set	16,613	3046511
BR 461 Seismic Brace Section L: 8000	8000	2,5	Set	18,091	3046512



# 9.5 Y

**BR461** 

X

#### **Assembly Includes**

Χ

- 2,5 mm 41x41 Binrak steel channel Hot-dip galvanize finish
- Seismic brace ceiling attachment special zinc finish
- M10X70 bolt
- M10 Fiber nut

#### Please indicate order code in your orders.

- 4000 mm and over 4000 mm orders should be attached
- $\blacksquare$  Material weights are approximate values, it can variate  $\pm 10\%$ .
- Please call us for non-standard components.





Description	Applicable Rod Size	Order Unit	Weight (kg/set)	Order Code
Seismic Rod Attacment (Secure Bolt) M8-M12	M8/M10/M12	Set	1,000	3046513
Seismic Rod Attacment (Secure Bolt) M14-20	M14/M16/M20	Set	0,966	3046514

#### Seismic Rod Attacment (Secure Bolt) M8-M12



#### Seismic Rod Attacment (Secure Bolt) M14-20



#### M8-M12 Set Includes

- M10X70 secure head-off bolt
- M10X70 bolt
- M10X35 bolt
- M10X45 bolt
- M10 spring nut
- 2 pcs M10 fiber nut
- Seismic rod fixing assembly Special zinc finish
- Seismic rod connection piece Special zinc finish

#### M14-M20 Set Includes

- M10X70 secure head-off bolt
- M10X70 bolt
- M10X35 bolt
- M10X45 bolt
- M10 spring nut
- 2 pcs M10 fiber nut
- Seismic rod fixing assembly Special zinc finish
- Seismic rod connection piece Special zinc finish

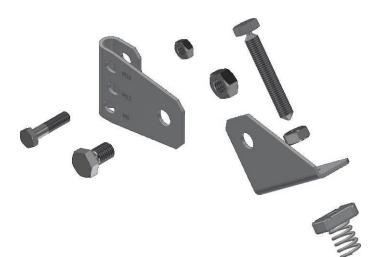
■ Material weights are approximate values, it can variate ±10%.





Description	Applicable	Order	Weight	Order
	Rod Size	Unit	(kg/set)	Code
Seismic Rod Set	M8/M10/M12	Set	0,381	3048465

#### Seismic Rod Set



#### **Set Includes**

- M12X30 bolt
- M8 fiber nut
- M12 flanged nut
- M10 fiber nut
- Seismic brace ceiling
- M8X30 bolt
- M10X70 secure head-off bolt
- M10 spring nut

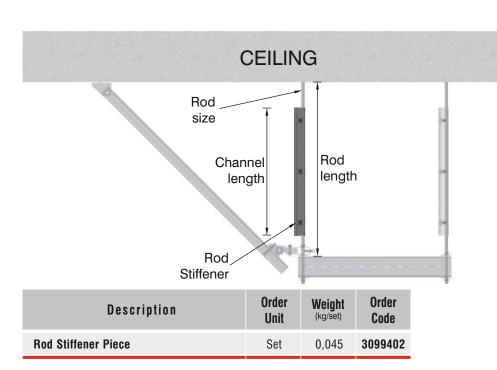


- Please indicate order code in your orders.
- $\blacksquare$  Material weights are approximate values, it can variate  $\pm 10\%$ .

#### ▶ 4. Products



Description	Rod Size	Rod Length	Channel Length (mm)	Channel Thickness (mm)	Stiffener Quantity	Order Unit	Weight (kg/set)	Order Code
Seismic Rod Stiffener Set (M8X700)	M8	700	500	2,5	3	Set	1,625	3046531
Seismic Rod Stiffener Set (M8X800)	M8	800	600	2,5	4	Set	1,970	3046624
Seismic Rod Stiffener Set (M8X900)	M8	900	700	2,5	4	Set	2,266	3046625
Seismic Rod Stiffener Set (M8X1000)	M8	1000	800	2,5	5	Set	2,610	3046626
Seismic Rod Stiffener Set (M8X1100)	M8	1100	900	2,5	5	Set	2,906	3046627
Seismic Rod Stiffener Set (M8X1200)	M8	1200	1000	2,5	5	Set	3,202	3046628
Seismic Rod Stiffener Set (M8X1300)	M8	1300	1100	2,5	6	Set	3,547	3046629
Seismic Rod Stiffener Set (M8X1400)	M8	1400	1200	2,5	6	Set	3,842	3046630
Seismic Rod Stiffener Set (M8X1500)	M8	1500	1300	2,5	7	Set	4,187	3046631
Seismic Rod Stiffener Set (M8X1600)	M8	1600	1400	2,5	7	Set	4,483	3046632
Seismic Rod Stiffener Set (M8X1700)	M8	1700	1500	2,5	8	Set	4,828	3046633
Seismic Rod Stiffener Set (M8X2200)	M8	2200	2000	2,5	10	Set	6,404	3046634
Seismic Rod Stiffener Set (M8X2700)	M8	2700	2500	2,5	12	Set	7,981	3046635
Seismic Rod Stiffener Set (M8X3200)	M8	3200	3000	2,5	14	Set	9,558	3046636



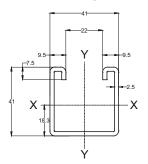
#### **Rod Stiffener**



#### **Rod Stiffener Set Includes**

- M8X40 bolt (see table for quantity)
- Rod stiffener pieces (see table for quantity)
   Special zinc finish
- BR 461 steel channel (see table for channel length) Hot-dip galvanize finish

#### **BR461**

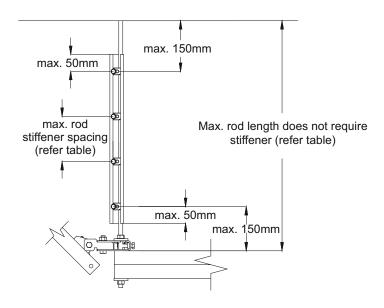


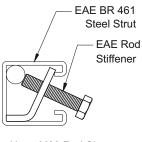
#### **Rod Stiffener Pieces**

- M8X40 bolt
- Rod Stiffener piece with special zinc finish
- Please indicate order code in your orders.
- Material weights are approximate values, it can variate ±10%.

#### ▶▶4. Products







Up to M20 Rod Sizes

Rod Size	Max. Rod Length Without Stiffener  (mm)	Max. Spacing Between Stiffener (mm)
M8	300	225
M10	475	325
M12	625	450
M16	775	575
M20	925	700





- Please indicate order code in your orders.
- $\blacksquare$  Material weights are approximate values, it can variate  $\pm 10\%$ .



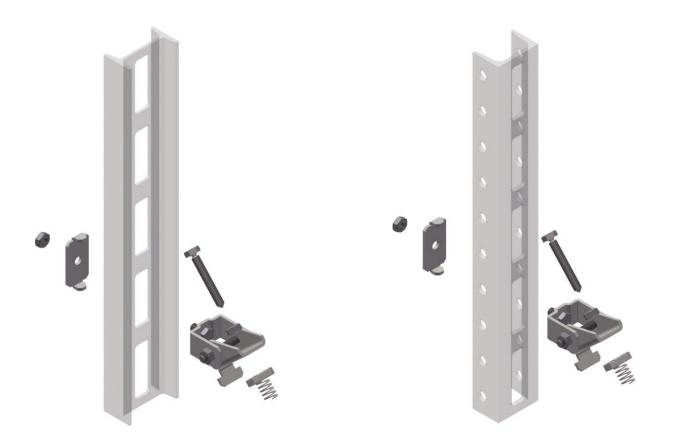


Description	Order	Weight	Order
	Unit	(kg/set)	Code
Seismic ID-UD Longitudinal Connection Set (Secure Bolt)	Set	0,584	3046517

## Seismic ID-UD Longitudinal Connection Set (Secure Bolt)



- M10X70 secure head-off bolt
- M10X70 bolt
- M10X30 bolt
- 2 pcs M10 nut
- M10 fiber nut
- M10 spring nut
- ID-UD seismic washer Special zinc finish
- Seismic U connection assembly Special zinc finish



- Please indicate order code in your orders.
- Material weights are approximate values, it can variate ±10%.





Description	Order	Weight	Order
	Unit	(kg/set)	Code
Seismic ID Lateral Connection Set (Secure Bolt)	Set	0,690	3046518

#### Seismic ID Lateral Connection Set (Secure Bolt)



- M10X70 secure head-off bolt
- M10X60 bolt
- 2 pcs M10X30 bolt
- M10 spring nut
- M10 fiber nut
- 3 pcs M10 nut
- 2 pcs ID seismic connection piece Special zinc finish
- Seismic length adjustment piece Special zinc finish



- Please indicate order code in your orders.
- $\blacksquare$  Material weights are approximate values, it can variate  $\pm 10\%$ .



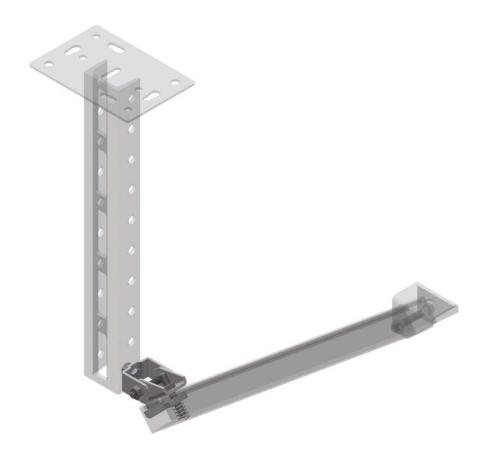


Description	Order	Weight	Order
	Unit	(kg/set)	Code
Seismic UD Lateral Connection Set (Secure Bolt)	Set	0,510	3046519

## Seismic UD Lateral Connection Set (Secure Bolt)



- M10X70 secure head-off bolt
- M10X70 bolt
- M10X30 bolt
- 2 pcs M10 nut
- M10 fiber nut
- M10 spring nut
- Seismic U connection assembly Special zinc finish



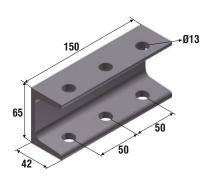
- Please indicate order code in your orders.
- $\blacksquare$  Material weights are approximate values, it can variate  $\pm 10\%$ .

#### ▶▶4. Products



#### Hot-dip Galvanize (EN ISO 1461)

Description	L (mm)	Order Unit	Weight (kg/pcs.)	Order Code
UDY 150	150	Piece	1,006	3008376

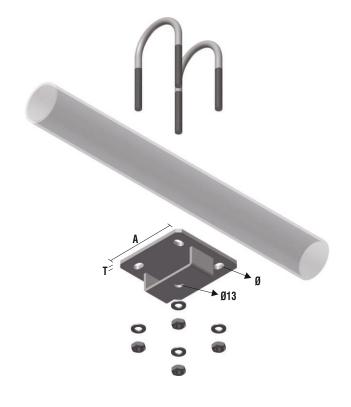




Description	A (mm)	T (mm)	Ø (mm)	Order Unit	Weight (kg/set)	Order Code
Seismic Pipe Beam Hanger DN50 (2")	115	6	11	Set	1,249	3046525
Seismic Pipe Beam Hanger DN65 (2 1/2")	125	6	11	Set	1,429	3046526
Seismic Pipe Beam Hanger DN80 (3")	150	6	13	Set	2,050	3046527
Seismic Pipe Beam Hanger DN100 (4")	180	6	13	Set	2,684	3046528
Seismic Pipe Beam Hanger DN125 (5")	200	6	13	Set	3,190	3046529
Seismic Pipe Beam Hanger DN150 (6")	250	8	18	Set	6,499	3046530

#### **Set Includes**

- 2 pcs U-bolt
- 4 pcs nut
- 4 pcs washer
- Seismic pipe beam plate Hot-dip galvanize finish





- Please indicate order code in your orders.
- $\blacksquare$  Material weights are approximate values, it can variate  $\pm 10\%$ .



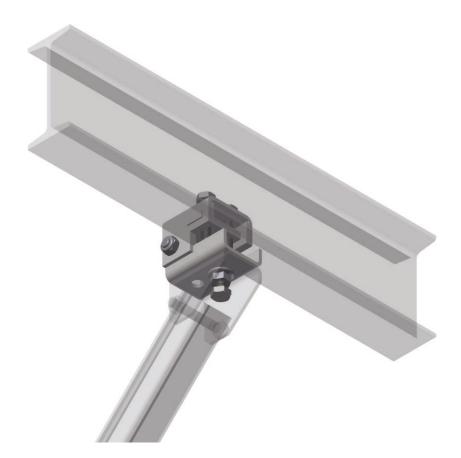


Description	Compatible Steel	Order	Weight	Order
	Profile Size	Unit	(kg/set)	Code
Seismic Steel Beam Hanger (Secure Bolt)	U80,I120 and upper	Set	0,880	3046523

#### Seismic Steel Beam Hanger (Secure Bolt)



- 3 pcs M10X70 secure head-off bolt
- 2 pcs M10X20 bolt
- 2 pcs M10 fiber nut
- M10 nut
- Beam hanger nut Special zinc finish
- Beam hanger assembly Special zinc finish



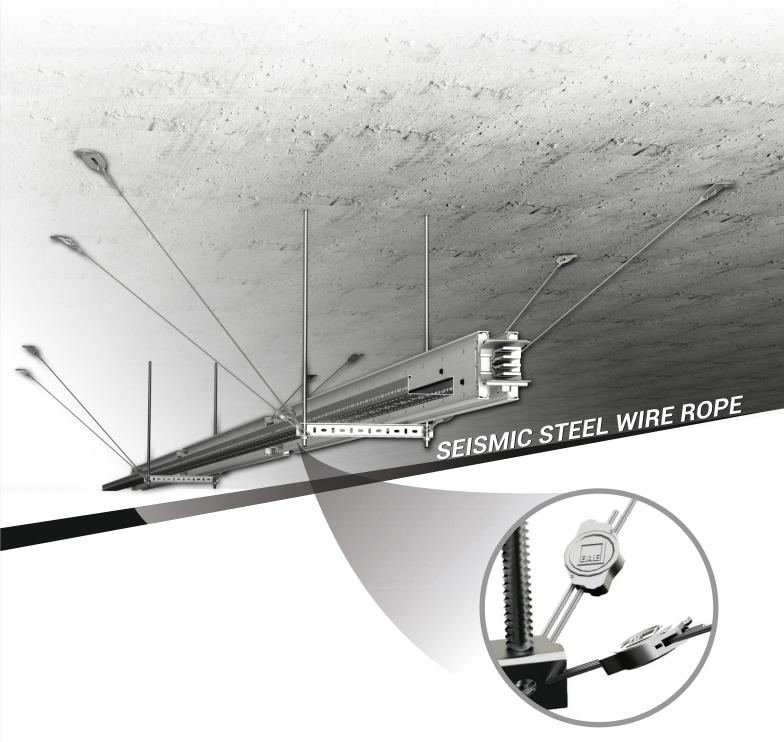
- Please indicate order code in your orders.
- Material weights are approximate values, it can variate  $\pm 10\%$ .





## Wire Rope Specification

	No:2	No:3	No:4
Diameter (mm)	2 mm	3 mm	4,8 mm
Wire Configuration	7x7	7x7	7x7
Min. Breaking Load (Kg)	260	580	1400
Max. Safety Work Weight (Kg)	50	110	250
Tensile Strength (Nmm²)	1750	1750	1750



#### ▶▶4. Products



#### Seismic Steel Wire Rope Set

Description	Order Code
No:2 - L=1 Meter Set with Ceiling Attachment	2064287
No:2 - L=2 Meter Set with Ceiling Attachment	2064288
No:2 - L=3 Meter Set with Ceiling Attachment	2064289
No:2 - L=5 Meter Set with Ceiling Attachment	2064290
No:2 - L=8 Meter Set with Ceiling Attachment	2064291
No:3 - L=1 Meter Set with Ceiling Attachment	2064292
No:3 - L=2 Meter Set with Ceiling Attachment	2064293
No:3 - L=3 Meter Set with Ceiling Attachment	2064294
No:3 - L=5 Meter Set with Ceiling Attachment	2064295
No:3 - L=8 Meter Set with Ceiling Attachment	2064296
No:4 - L=1 Meter Set with Ceiling Attachment	2064297
No:4 - L=2 Meter Set with Ceiling Attachment	2064298
No:4 - L=3 Meter Set with Ceiling Attachment	2064299
No:4 - L=5 Meter Set with Ceiling Attachment	2064300
No:4 - L=8 Meter Set with Ceiling Attachment	2064301

No:4 - L=8 Meter Set with Ceiling Attachment	2064301	
Sets include ;		Sets in
<ul> <li>Ordered length of steel rope</li> </ul>		<ul><li>Order</li></ul>

- Ordered size of special clamp
- Aluminum Sleeves
- Thimble
- Ceiling Attachment

Description	Order Code
No: 2 - L = 1 Meter Set	2065271
No: 2 - L = 2 Meter Set	2065272
No: 2 - L = 3 Meter Set	2065273
No: 2 - L = 5 Meter Set	2065274
No: 2 - L = 8 Meter Set	2065276
No: 3 - L = 1 Meter Set	2065277
No : 3 - L = 2 Meter Set	2065278
No : 3 - L = 3 Meter Set	2065279
No : 3 - L = 5 Meter Set	2065280
No : 3 - L = 8 Meter Set	2065281
No : 4 - L = 1 Meter Set	2065282
No : 4 - L = 2 Meter Set	2065283
No : 4 - L = 3 Meter Set	2065284
No : 4 - L = 5 Meter Set	2065285
No : 4 - L = 8 Meter Set	2065286

- Sets include;
   Ordered length of steel rope
- Ordered size of special clamp
- Aluminum Sleeves
- Thimble





## **EAE SEISMIC COMPONENTS**



Spring Nut Available for bolt or rod sizes of m6 to m12



**DIN 933 8.8 Bolts** Various sizes



Hexagon Nut Available for bolt or rod sizes of m6 to m16



Seismic Brace Rod Attachment Compatible for rod sizes m8 to m12 or M14 to m20



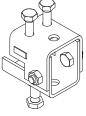
Secure Head-off Bolt Available sizes of m10 and m12



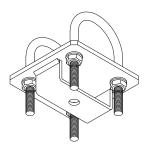
Seismic Brace Ceiling Attachment Compatible for Anchor sizes up to m12



Rod Stiffener Compatible up to M20 rod sizes



**EAE Steel Beam** Fastener Compatible for I120, U80 and bigger steel beams



EAE Pipe Beam Fastener Available sizes for DN50 to DN150 Pipe Beams





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#### ▶► 5. Technical Information



## **DESIGN PROCEDURE**

Design procedure given here is for determining brace spacing and trapeze width of the distribution system being braced. Calculations examples are according to IBC® 2012. These calculations are for determining seismic acceleration. The tables given here are however showing universal system allowable loads. Therefore, can be applied to any building code. Please consult with a design professional for project specific brace layout.

Design process should follow steps below:

Trapeze Assembly Design Steps

Stage - 1 Trapeze Section

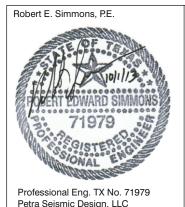
- 1 Determine system max. trapeze spacing.
- 2 Determine system dead load (operating load).
- 3 Determine system max. brace spacing.
- 4 Determine system max. horizontal seismic load.
- 5 Determine system max. vertical seismic load.
- 6 Determine combined loads and trapeze section.

Stage - 2 Rod

- 7 Determine threaded rod.
- 8 Determine rod stiffener usage.

Stage - 3 Brace

- 9 Determine brace section length and installation angle.
- 10 Determine brace section.
- 11 Determine brace anchor loads.
- 12 Determine brace anchor.



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#### ▶► 5. Technical Information



## STEP 1

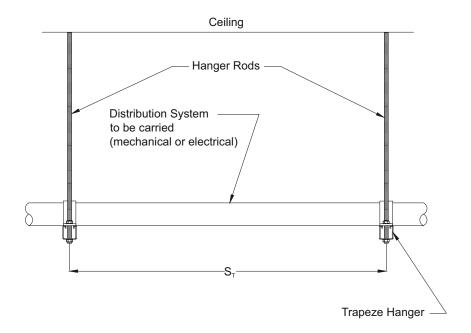
## **Determining Trapeze Spacing**

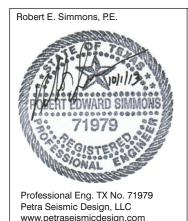
Maximum trapeze hanger spacings  $S_{\scriptscriptstyle T}$  should be determined by including but not limited to; governing regulations, technical specifications of the distribution system to be installed.

Consult with a project specialist for more information.

Most accepted trapeze spacing is 1.5m for most of the distribution system, including but not limited to; electrical cable trays, electrical bus ducts.

 $\textbf{S}_{\scriptscriptstyle T}$  : Maximum trapeze spacing in meters allowed by governing regulation or technical specification.





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#### ▶► 5. Technical Information



## STEP 2

## **Determining Dead Load**

Maximum operating vertical load D, should be determined using following calculation;

 $D = S_{T} \times Wt \times 1.15$ 

D : Component operating weight (operating vertical load,dead load).
 S<sub>τ</sub> : Maximum trapeze spacing in meters allowed by governing regulatio

5 : Maximum trapeze spacing in meters allowed by governing regulation or technical specification.

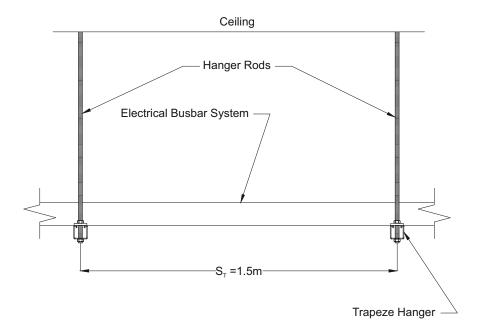
Wt : Operating weight of the distribution system per meter.

1.15 factor stands for applying self weight of the trapeze assembly.

#### Example 1:

The system to be braced is an electrical busbar system that weigh 0.588 kN per meter. Technical specification of the busbar system limits the maximum support spacing to 1.5 meters. System maximum dead load will be;

D =  $1.5 \times 0.588 \times 1.15 = 1.015 \text{ kN's}$ .







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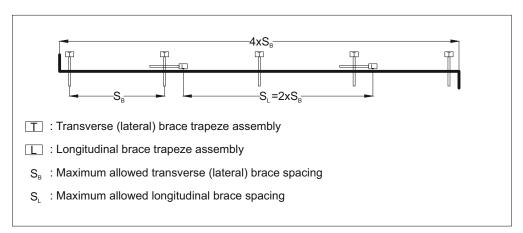
## STEP 3

## **Determining Brace Spacing**

Generally maximum transverse (lateral) sway brace spacing is 12m for fire protection sprinkler systems, pipes, conduits and 9m for cable trays and busbar systems. Most accepted spacing of transverse (lateral) braces for HVAC ductworks are 9m according to 1998 Seismic Restraint Guidelines for Mechanical Systems (SMACNA). Longitudinal brace spacing is two times of transverse (lateral) span. Please note that these spacings are mostly accepted values by the specifications and codes. Project specific criterias may vary internationally.

Refer NFPA 13 for more detailed information on seismic bracing layout on fire protection systems.

Design professionals can be consulted for bracing layouts. Following sections include the data needed for design specialists. For more information, contact EAE customer relations or visit www.eae.com.tr.



Example Layout of Max. Brace spacings for Suspended Distribution Systems

Suspended distribution system to be braced	Max. trasverse brace spacing S <sub>B</sub>	Max. longitudinal brace spacing S <sub>⊾</sub>
Steel and copper pipe with welded, brazed, grooved or screwed connections	12 m	24 m
PVC of PVDF pipe with solvent-welded connections	6 m	12 m
No-hub Pipe with shield and clamp connections	6 m	12 m
Sheet metal ductwork	9 m	18 m





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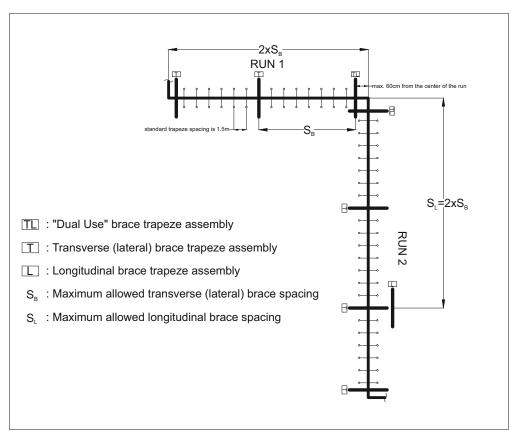
## STEP 3

### **Determining Brace Spacing**

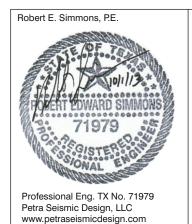
This section is for making bracing layouts easier. Figures shown in this section are provided for all trapeze assemblies that carry any specific distribution system. Conditions taken into count is for worst case scenario for 1.5m trapeze span and  $S_a$  lateral brace spacing.

#### Dual Use Transverse (lateral) Brace:

A "Dual Use" transverse (lateral) brace works both as lateral brace of the distribution system run installed, and as the longitudinal brace of the neighboring run. Example layout for a "Dual Use" brace is given below.



General Bracing Layout



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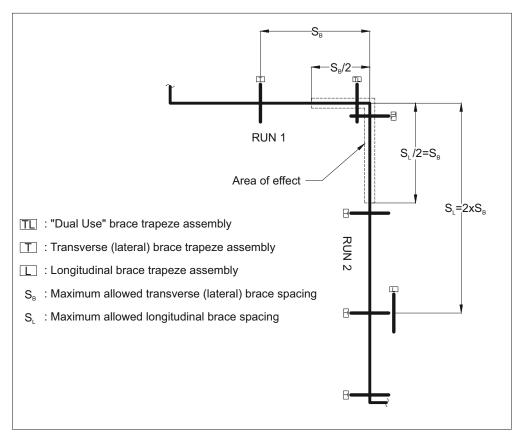
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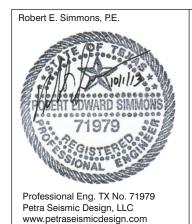
## STEP 3

### **Determining Brace Spacing**

At the maximum allowed brace spacing and standard 1.5m trapeze span, a "Dual Use" trapeze brace assembly should withstand 1.5m of dead load plus 3/2  $S_{\scriptscriptstyle B}$  meters of earthquake load of the distribution system. Examples given in following sections are provided with that respect. Refer to concerned table for load combinations and allowable loads for the trapeze assembly.



"Dual Use" Brace Area of Effect



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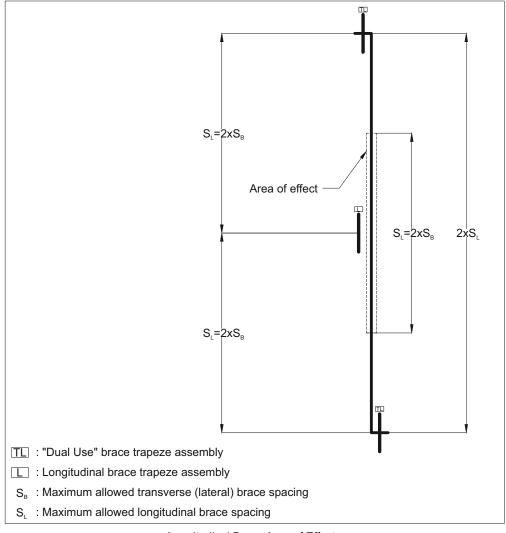


## STEP 3

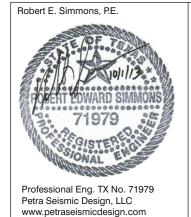
### **Determining Brace Spacing**

#### Longitudinal Brace:

Longitudinal Trapeze Brace assembly at 1.5m standard trapeze span, and  $S_L$  maximum allowed longitudinal brace spacing should withstand 1.5m of dead load plus  $S_L$  meters of earthquake load. Examples given in following section are provided with that respect. Refer to concerned table for load combinations and allowable loads for the trapeze assembly.



Longitudinal Brace Area of Effect



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## STEP 4

### **Determining Horizontal Seismic Load**

System acceleration "G", can be determined by use of any building code. Below calculation examples are according to IBC® 2012 governed by ICC®. IBC® referred calculations and constants are from ASCE/SEI 7-10 chapter 13.

G : Horizontal seismic design acceleration is equal to  $F_P / W_P$ .

Horizontal seismic design force:

$$F_{\text{P}} = \underbrace{0.4a_{\text{P}}S_{\text{DS}}W_{\text{P}}}_{\text{C}}\left(1 + 2\frac{z}{h}\right) \qquad \qquad \text{where,} \quad 0.3S_{\text{DS}}I_{\text{P}}W_{\text{P}} \leqslant F_{\text{P}} \leqslant 1.6S_{\text{DS}}I_{\text{P}}W_{\text{P}} \leqslant S_{\text{DS}}I_{\text{P}}W_{\text{P}} \leqslant S_{\text{DS}}I_{\text$$

F<sub>D</sub>: Horizontal seismic design force.

S<sub>pc</sub>: Spectral acceleration, short period.

: Component amplification factor varies from 1.00 to 2.50 (ASCE/SEI 7-10 Table 13.5-1 or 13.6-1).

I<sub>P</sub> : Component importance factor that varies from 1.00 to 1.50 (ASCE/SEI 7-10 13.1.3).

W<sub>P</sub> : Component operating weight.

R<sub>p</sub>: Component response modification factor that varies from 1.00 to 12 (ASCE/SEI 7-10 Table 13.5-1 or 13.6-1).

z : Height in structure of point of attachment of component with respect to the base. For items at or below base, z shall be taken as 0. The value z/h need not exceed 1.0.

h : Average roof height of structure with respect to the base.

S<sub>s</sub>: Spectral response acceleration.

F<sub>a</sub> : Site coefficient.

#### Example 2:

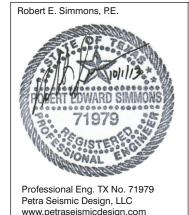
The trapeze system in example 1 is on a basement floor of a building located at Istanbul/TURKEY. The distribution system carried by the trapeze assembly is an electrical busbar system, that supplies fire pumps. The system seismic acceleration "G" should be:

"G" value is smaller than the minimum value, therefore system acceleration "G" will be:

G = 0.495

#### Notes:

Values  $a_P$ ,  $R_P$  are selected from ASCE/SEI 7-10 Table 13.6-1.  $I_P$  is determined as 1.50 for electrical system that supplies an emergency system.  $S_{DS}$  is determined by selecting  $S_S$  values from US COE 1998 international locations, and with soil condition unknown, site coefficient  $F_a$  is taken as 1.00 according to IBC $^{\circ}$  2012 Table 1613.3.3(1).



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## STEP 4

## **Determining Horizontal Seismic Load**

Maximum brace spacings must be considered when determining system seismic design load. Once design acceleration "G" is determined, horizontal seismic loads of the system should be determined using following calculation:

 $F_{Plmax} = S_L x Wt x 1.15 x G$  $F_{Plmax} = 3/2S_B x Wt x 1.15 x G$ 

 $F_{\mbox{\tiny Plmax}}$ : Maximum longitudinal seismic design force.

F<sub>Ptmax</sub>: Maximum transverse (lateral) seismic design force.

S<sub>L</sub>: Maximum longtudinal brace spacing in meters allowed by governing code or technical specification.

technical specification.

 $S_{\scriptscriptstyle B}$  : Maximum transverse (lateral) brace spacing in meters allowed by governing code or technical specification.

Wt : Operating weight of the distribution system per meter.

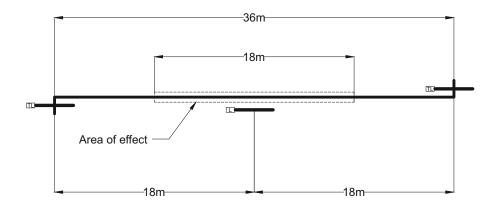
G: Horizontal seismic design acceleration.

1.15 factor stands for applying self weight of the trapeze assembly.

#### Example 3:

Maximum brace spacing of the busbar system described in example 2 is 9m for lateral bracing and 18m for longitudinal bracing. And the weight of the busbar system is 0.588 kN/m. The system maximum horizontal seismic design forces will be:

 $F_{Plmax}$  = 18x0.588x1.15x0.495 = 6.024 kN's.





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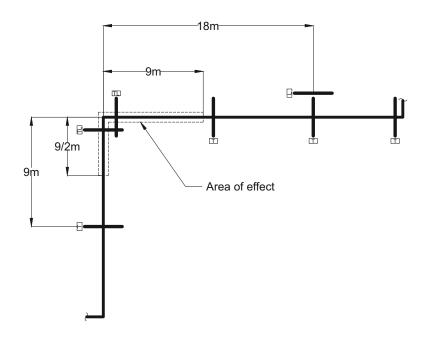


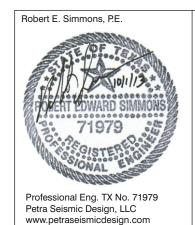
## STEP 4

## **Determining Horizontal Seismic Load**

Example 3 continue:

 $F_{Ptmax} = 3/2x9x0.588x1.15x0.495 = 4.518 \text{ kN's}.$ 





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## STEP 5

## **Determining Vertical Seismic Load**

Seismic vertical loads can be determided by use of any building code. Below calculation examples are according to IBC® 2012 governed by ICC®. IBC® referred calculations and constants are from ASCE/SEI 7-10 chapter 13.

### Seismic Vertical Design Force:

 $F_{v} = 0.2 \times S_{DS} \times D$ 

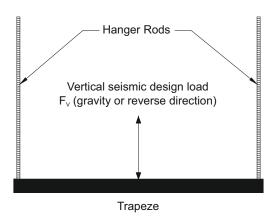
F<sub>v</sub>: Vertical sysmic design force.S<sub>ns</sub>: Spectral acceleration, short period.

D : Component operating weight (operating vertical load, dead load).

#### Example 4:

Vertical seismic design force of the system described in previous examples will be:

 $F_{v} = 0.2 \times 1.1 \times 1.015 = 0.224 \text{ kN/s}.$ 





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## STEP 6

### **Determining Trapeze Section**

### **Loading Conditions:**

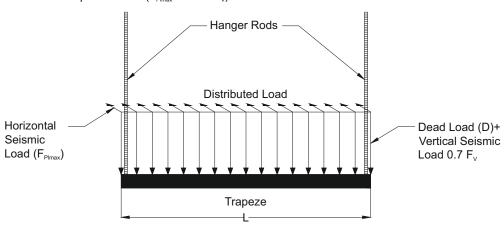
Allowable loads given in this section are calculated according to AISI 1999 allowable stress design. Load combination used is as per specified in ASCE/SEI 7-10 2.4.1 combination 5 (D + 0.7E).

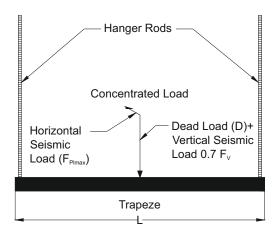
Loading diagram given below is used for uniform loading and concentrated loading.

Refer to the loading combination notes for exact loading force directions.

D : Dead Loads

E : Earthquake Loads (F<sub>Plmax</sub> and 0.7F<sub>V</sub>)









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## STEP 6

### **Determining Trapeze Section**

#### Loading Combinations:

Once all loads are determined, the trapeze section will be chosen from the tables on pages A6-3 to A6-17. Allowable vertical force values in tables are according to flexural strength of the section in x-x axis. Allowable horizontal seismic load values in tables are according to flexural strength of the section in y-y axis divided by 0.7 for ASD combination. Final combination of loads should satisfy below calculation\*.

Total vertical load		Total horizontal seismic load		1
Allowable vertical load	т	Allowable horizontal seismic load	~	'

#### Example 5:

Trapeze section of the system is determined BR 461 section with lenght of 300 mm in concentrated loading. The section is:

 $[(0.7F_v + D) / Allowable vertical load] + [F_{Plmax} / Allowable horizontal seismic load] <math>\leq 1$ 

 $[((0.7x0.224+1.015)/9.520] + [6.024/11.750] = 0.64 \le 1 \quad , ok.$ 

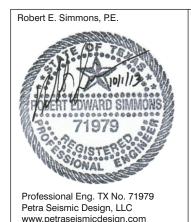
 $F_{\nu}$ : Vertical seismic design force.

D : Component operating weight (operating vertical load,dead load).

F<sub>Plmax</sub>: Maximum longitudinal seismic design force.

For allowable load values\*\* see tables on pages A6-3 to A6-17.

<sup>\*\*</sup>The values are calculated according to AISI 1999 allowable stress design (ASD) and the material used is DIN10025-P2 S235JR.



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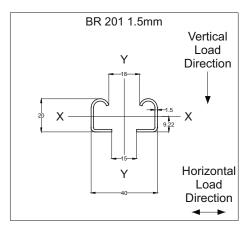
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<sup>\*</sup> The design worse case scenario for the trapeze section is under maximum longitudinal seismic design forces. Therefor, trapeze section should be determined by the longitudinal design forces.

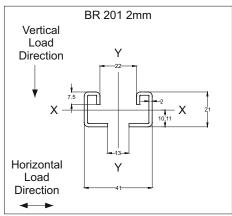
### ▶► 5. Technical Information



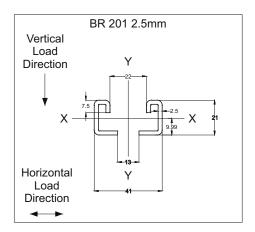
# STEP 6



BR 201-1,5mm Steel Section				
Lamela	Allowable \	ertical Load	oad Allowable Horizontal Seismic Load	
Lenght	Concentrated	Distributed	Concentrated	Distributed
mm	kN	kN	kN	kN
300	1,042	2,084	0,803	1,606
400	0,781	1,563	0,803	1,606
500	0,625	1,250	0,803	1,606
600	0,521	1,042	0,803	1,606
700	0,447	0,893	0,803	1,606
800	0,391	0,781	0,803	1,606
900	0,347	0,695	0,803	1,606
1000	0,313	0,625	0,803	1,606
1100	0,284	0,568	0,803	1,606
1200	0,260	0,521	0,803	1,606
1300	0,240	0,481	0,803	1,606
1400	0,223	0,447	0,803	1,606
1500	0,208	0,417	0,803	1,606
1600	0,195	0,391	0,803	1,606
1700	0,184	0,368	0,803	1,606
1800	0,174	0,347	0,803	1,606
1900	0,165	0,329	0,803	1,606
2000	0,156	0,313	0,803	1,606
3000	0,104	0,208	0,573	1,147



	BR 201-2mm Steel Section			
Lenght	İzin Verilen Düşey Yük		Allowable Horizon	ntal Seismic Load
Lengni	Concentrated	Distributed	Concentrated	Distributed
mm	kN	kN	kN	kN
300	2,553	5,107	7,481	14,962
400	1,915	3,830	5,611	11,221
500	1,532	3,064	4,489	8,977
600	1,277	2,553	3,740	7,481
700	1,094	2,189	3,206	6,412
800	0,958	1,915	2,805	5,611
900	0,851	1,702	2,494	4,987
1000	0,766	1,532	2,244	4,489
1100	0,696	1,393	2,040	4,081
1200	0,638	1,277	1,870	3,740
1300	0,589	1,179	1,726	3,453
1400	0,547	1,094	1,603	3,206
1500	0,511	1,021	1,496	2,992
1600	0,479	0,958	1,403	2,805
1700	0,451	0,901	1,320	2,640
1800	0,426	0,851	1,247	2,496
1900	0,403	0,806	1,181	2,362
2000	0,383	0,766	1,122	2,244
3000	0,255	0,511	0,748	1,496



BR 201-2,5mm Steel Section				
Lenght	Allowable \	/ertical Load	Allowable Horizo	ntal Seismic Load
Lengni	Concentrated	Distributed	Concentrated	Distributed
mm	kN	kN	kN	kN
300	2,995	5,989	9,172	18,343
400	2,246	4,492	6,879	13,757
500	1,797	3,594	5,503	11,006
600	1,497	2,995	4,586	9,172
700	1,283	2,567	3,931	7,861
800	1,123	2,246	3,439	6,879
900	0,992	1,996	3,057	6,114
1000	0,898	1,797	2,751	5,503
1100	0,817	1,633	2,501	5,003
1200	0,749	1,497	2,293	4,586
1300	0,691	1,382	2,117	4,233
1400	0,642	1,283	1,965	3,931
1500	0,599	1,198	1,834	3,669
1600	0,562	1,123	1,720	3,439
1700	0,528	1,057	1,619	3,237
1800	0,499	0,998	1,529	3,057
1900	0,473	0,946	1,448	2,896
2000	0,449	0,898	1,376	2,751
3000	0,299	0,599	0,917	1,834





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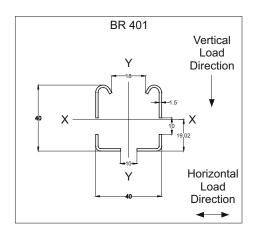
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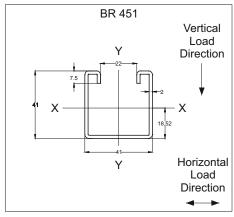
### ▶► 5. Technical Information



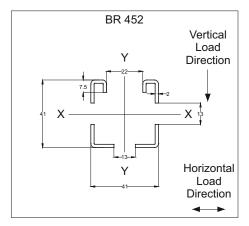
# STEP 6



		DD 404 C4I	C4!	
	BR 401 Steel Section			
Lenght	Allowable Ve	rtical Load	Allowable Horizo	ntal Seismic Load
Lengin	Concentrated	Distributed	Concantrated	Distributed
mm	kN	kN	kN	kN
300	3,260	6,519	3,856	7,712
400	2,445	4,890	2,892	5,784
500	1,956	3,912	2,313	4,627
600	1,630	3,260	1,928	3,856
700	1,397	2,794	1,652	3,305
800	1,222	2,445	1,446	2,892
900	1,087	2,179	1,285	2,571
1000	0,978	1,956	1,157	2,313
1100	0,889	1,778	1,052	2,103
1200	0,815	1,630	0,964	1,928
1300	0,752	1,504	0,890	1,780
1400	0,699	1,397	0,826	1,652
1500	0,652	1,304	0,771	1,542
1600	0,611	1,222	0,723	1,446
1700	0,575	1,150	0,680	1,361
1800	0,543	1,087	0,643	1,285
1900	0,515	1,029	0,609	1,218
2000	0,489	0,978	0,578	1,157
3000	0,326	0,652	0,386	0,771



	BR 451 Steel Section			
Lenght	Allowable Ve	rtical Load	Allowable Horizo	ontal Seismic Load
Lengin	Concentrated	Distributed	Concentrated	Distributed
mm	kN	kN	kN	kN
300	7,780	15,560	9,723	19,446
400	5,835	11,670	8,478	16,956
500	4,668	9,336	6,782	13,565
600	3,890	7,780	5,652	11,304
700	3,334	6,669	4,844	9,689
800	2,918	5,835	4,239	8,478
900	2,593	5,187	3,768	7,536
1000	2,334	4,668	3,391	6,782
1100	2,122	4,244	3,083	6,166
1200	1,945	3,890	2,826	5,652
1300	1,795	3,591	2,609	5,217
1400	1,667	3,334	2,422	4,844
1500	1,556	3,112	2,261	4,522
1600	1,459	2,918	2,119	4,239
1700	1,373	2,746	1,995	3,990
1800	1,297	2,593	1,884	3,768
1900	1,228	2,457	1,785	3,570
2000	1,167	2,334	1,696	3,391
3000	0.778	1,556	1,130	2,261



	BR 452 Steel Section			
Lenght	Allowable Ve		Allowable Horizo	ontal Seismic Load
Lengni	Concentrated	Distributed	Concentrated	Distributed
mm	kN	kN	kN	kN
300	7,172	14,344	8,400	16,800
400	5,379	10,758	6,300	12,600
500	4,303	8,606	5,040	10,080
600	3,586	7,172	4,200	8,400
700	3,074	6,147	3,600	7,200
800	2,689	5,379	3,150	6,300
900	2,391	4,781	2,800	5,600
1000	2,152	4,303	2,520	5,040
1100	1,956	3,912	2,291	4,582
1200	1,793	3,586	2,100	4,200
1300	1,655	3,310	1,938	3,877
1400	1,537	3,074	1,800	3,600
1500	1,434	2,869	1,680	3,360
1600	1,345	2,689	1,575	3,150
1700	1,266	2,531	1,482	2,965
1800	1,195	2,391	1,400	2,800
1900	1,132	2,265	1,326	2,653
2000	1,076	2,152	1,260	2,520
3000	0,717	1,434	0,840	1,680

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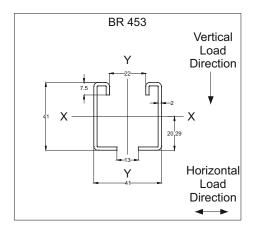
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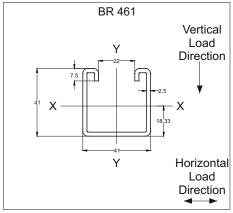
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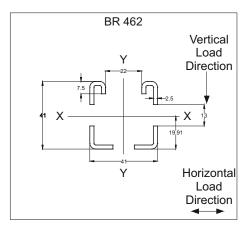
# STEP 6



		BR 453 Steel	Section	
1	Allowable \	/ertical Load	Allowable Horizontal Seismic L	
Length	Concentrated	Distributed	Concentrated	Distributed
mm	kN	kN	kN	kN
300	7,287	14,574	9,723	19,446
400	5,465	10,930	8,438	16,877
500	4,372	8,744	6,751	13,501
600	3,643	7,287	5,626	11,251
700	3,123	6,246	4,822	9,644
800	2,733	5,465	4,219	8,438
900	2,429	4,858	3,750	7,501
1000	2,186	4,372	3,375	6,751
1100	1,987	3,975	3,068	6,137
1200	1,822	3,643	2,813	5,626
1300	1,682	3,363	2,596	5,193
1400	1,561	3,123	2,411	4,822
1500	1,457	2,915	2,250	4,500
1600	1,366	2,733	2,110	4,219
1700	1,286	2,572	1,985	3,971
1800	1,214	2,429	1,875	3,750
1900	1,151	2,301	1,776	3,553
2000	1,093	2,186	1,688	3,375
3000	0,729	1,457	1,125	2,250



BR 461 Steel Section				
	Allowable \	/ertical Load	Allowable Horizon	ntal Seismic Load
Length	Concentrated	Distributed	Concentrated	Distributed
mm	kN	kN	kN	kN
300	9,520	19,039	11,750	23,500
400	7,140	14,280	10,349	20,697
500	5,712	11,424	8,279	16,558
600	4,760	9,520	6,899	19,798
700	4,080	8,160	5,913	11,827
800	3,570	7,140	5,174	10,349
900	3,173	6,346	4,599	9,199
1000	2,856	5,712	4,139	8,279
1100	2,596	5,193	3,763	7,526
1200	2,380	4,760	4,450	6,899
1300	2,197	4,394	3,184	6,368
1400	2,040	4,080	2,957	5,913
1500	1,904	3,808	2,760	5,519
1600	1,785	3,570	2,587	5,174
1700	1,680	3,360	2,435	4,870
1800	1,587	3,173	2,300	4,599
1900	1,503	3,006	2,179	4,357
2000	1,428	2,856	2,070	4,139
3000	0,952	1,904	1,380	2,760



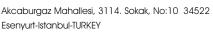
BR 462 Steel Section				
Length	Allowable \	/ertical Load	Allowable Horizontal Seismic Loa	
Length	Concentrated	Distributed	Concentrated	Distributed
mm	kN	kN	kN	kN
300	8,719	17,438	10,174	20,348
400	6,539	13,079	7,631	15,261
500	5,231	10,463	6,104	12,209
600	4,360	8,719	5,087	10,174
700	3,737	7,473	4,360	8,721
800	3,270	6,539	3,815	7,631
900	2,906	5,813	3,391	6,783
1000	2,616	5,231	3,052	6,104
1100	2,378	4,756	2,775	5,550
1200	2,180	4,360	2,544	5,087
1300	2,012	4,024	2,348	4,696
1400	1,868	3,737	2,180	4,360
1500	1,744	3,488	2,035	4,070
1600	1,635	3,270	1,908	3,815
1700	1,539	3,077	1,795	3,591
1800	1,453	2,906	1,696	3,391
1900	1,377	2,753	1,606	3,213
2000	1,308	2,616	1,526	3,052
3000	0,872	1,744	1,017	2,035





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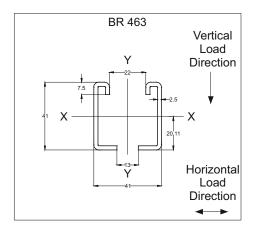
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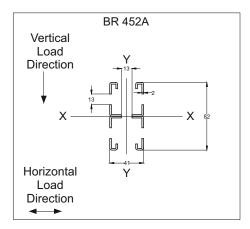
# STEP 6



BR 463 Steel Section				
1	Allowable V	/ertical Load	Allowable Horizo	ontal Seismic Load
Length	Concentrated	Distributed	Concentrated	Distributed
mm	kN	kN	kN	kN
300	8,889	17,779	11,750	23,500
400	6,667	13,334	10,298	20,596
500	5,334	10,667	8,238	16,477
600	4,445	8,889	6,865	13,730
700	3,810	7,619	5,884	11,769
800	3,334	6,667	5,149	10,298
900	2,963	5,926	4,577	9,154
1000	2,667	5,334	4,119	8,238
1100	2,424	4,849	3,745	7,489
1200	2,222	4,445	3,433	6,865
1300	2,051	4,103	3,169	6,337
1400	1,905	3,810	2,942	5,884
1500	1,778	3,556	2,746	5,492
1600	1,667	3,334	2,574	5,149
1700	1,569	3,137	2,423	4,846
1800	1,482	2,963	2,288	4,577
1900	1,404	2,807	2,168	4,336
2000	1,333	2,667	2,060	4,119
3000	0,889	1,778	1,373	2,746

	BR 451A
Vertical Load Direction	Υ
×	X 82
Horizontal Load Direction	¥ 41

	BR 451A Steel Section				
Length	Allowable \	/ertical Load	Allowable Horizontal Seismic Loa		
Length	Concentrated	Distributed	Concentrated	Distributed	
mm	kN	kN	kN	kN	
300	21,447	42,893	19,444	38,889	
400	16,085	32,170	16,956	33,911	
500	12,868	25,736	13,565	27,129	
600	10,723	21,447	11,304	22,608	
700	9,191	18,383	9,689	19,378	
800	8,043	16,085	8,478	16,956	
900	7,149	14,298	7,536	15,072	
1000	6,434	12,868	6,782	13,565	
1100	5,849	11,698	6,166	12,331	
1200	5,362	10,723	5,652	11,304	
1300	4,949	9,898	5,217	10,434	
1400	4,596	9,191	4,844	9,689	
1500	4,289	8,579	4,522	9,043	
1600	4,021	8,043	4,239	8,478	
1700	3,785	7,569	3,990	7,979	
1800	3,574	7,149	3,768	7,536	
1900	3,386	6,773	3,570	7,139	
2000	3,217	6,434	3,391	6,782	
3000	2,145	4,289	2,261	4,522	



	BR 452A Steel Section				
Length	Allowable Vertical Load		Allowable Horizontal Seismic Load		
Length	Concentrated	Distributed	Concentrated	Distributed	
mm	kN	kN	kN	kN	
300	18,436	36,872	16,800	33,600	
400	13,827	27,654	12,600	25,200	
500	11,062	22,123	10,080	20,160	
600	9,218	18,436	8,400	16,800	
700	7,901	15,802	7,200	14,400	
800	6,914	13,827	6,300	12,600	
900	6,145	12,291	5,600	11,200	
1000	5,531	11,062	5,040	10,080	
1100	5,028	10,056	4,582	9,164	
1200	4,609	9,218	4,200	8,400	
1300	4,254	8,509	3,877	7,754	
1400	3,951	7,901	3,600	7,200	
1500	3,687	7,374	3,360	6,720	
1600	3,457	6,914	3,150	6,300	
1700	3,253	6,507	2,965	5,929	
1800	3,073	6,145	2,800	5,600	
1900	2,911	5,822	2,653	5,305	
2000	2,765	5,531	2,520	5,040	
3000	1,844	3,687	1,680	3,360	





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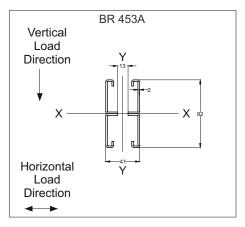
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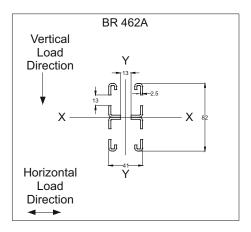
# STEP 6



	BR 453A Steel Section				
Longth	Allowable \	/ertical Load	Allowable Horizontal Seismic Lo		
Length	Concantrated	Distributed	Concantrated	Distributed	
mm	kN	kN	kN	kN	
300	21,443	42,885	19,444	38,889	
400	16,082	32,164	16,877	33,754	
500	12,866	25,731	13,502	27,003	
600	10,721	21,443	11,251	22,503	
700	9,190	18,379	9,644	19,288	
800	8,041	16,082	8,439	16,877	
900	7,148	14,295	7,501	15,002	
1000	6,433	12,866	6,751	13,502	
1100	5,848	11,696	6,137	12,274	
1200	5,361	10,721	5,626	11,251	
1300	4,948	9,897	5,193	10,386	
1400	4,595	9,190	4,822	9,644	
1500	4,289	8,577	4,501	9,001	
1600	4,021	8,041	4,219	8,439	
1700	3,784	7,568	3,971	7,942	
1800	3,574	7,148	3,750	7,501	
1900	3,386	6,771	3,553	7,106	
2000	3,216	6,433	3,375	6,751	
3000	2,144	4,289	2,250	4,501	

	BR 461A
Vertical Load Direction	Υ
×	X 82
Horizontal Load Direction	Y

	BR 461A Steel Section				
Length	Allowable \	/ertical Load	Allowable Horizontal Seismic Load		
Length	Concantrated	Distributed	Concantrated	Distributed	
mm	kN	kN	kN	kN	
300	26,720	53,440	23,500	47,000	
400	20,040	40,080	20,697	41,394	
500	16,032	32,064	16,558	33,115	
600	13,360	26,720	13,798	27,596	
700	11,451	22,903	11,827	23,654	
800	10,020	20,040	10,349	20,697	
900	8,907	17,813	9,199	18,397	
1000	8,016	16,032	8,279	16,558	
1100	7,287	14,575	7,526	15,052	
1200	6,680	13,360	6,899	13,798	
1300	6,166	12,332	6,368	12,737	
1400	5,726	11,451	5,913	11,827	
1500	5,344	10,688	5,519	11,038	
1600	5,010	10,020	5,174	10,349	
1700	4,715	9,431	4,870	9,740	
1800	4,453	8,907	4,599	9,199	
1900	4,219	8,438	4,357	8,715	
2000	4,008	8,016	4,139	8,279	
3000	2,672	5,344	2,760	5,519	



	BR 462A Steel Section					
Length	Allowable Vertical Load		Allowable Horizontal Seismic Load			
Length	Concantrated	Distributed	Concantrated	Distributed		
mm	kN	kN	kN	kN		
300	22,752	45,504	20,349	40,697		
400	17,064	34,128	15,261	30,523		
500	13,651	27,302	12,209	24,418		
600	11,376	22,752	10,174	20,349		
700	9,751	19,502	8,721	17,442		
800	8,532	17,064	7,631	15,261		
900	7,584	15,168	6,783	13,566		
1000	6,826	13,651	6,105	12,209		
1100	6,205	12,410	5,550	11,099		
1200	5,688	11,376	5,087	10,174		
1300	5,250	10,501	4,696	9,392		
1400	4,875	9,751	4,360	8,721		
1500	4,550	9,101	4,070	8,139		
1600	4,266	8,532	3,815	7,631		
1700	4,015	8,030	3,591	7,182		
1800	3,792	7,584	3,391	6,783		
1900	3,592	7,185	3,213	6,426		
2000	3,413	6,826	3,052	6,105		
3000	2,275	4,550	2,035	4,070		





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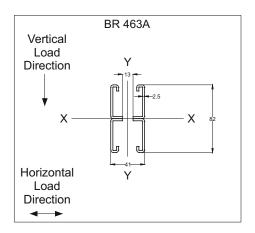
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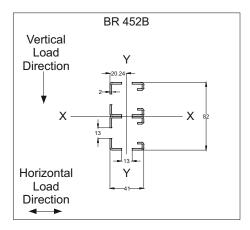
# STEP 6



	BR 463A Steel Section				
Length	Allowable \	ertical Load	Allowable Horizontal Seismic Load		
Length	Concantrated	Distributed	Concantrated	Distributed	
mm	kN	kN	kN	kN	
300	26,711	53,421	23,500	47,000	
400	20,033	40,066	20,596	41,191	
500	16,026	32,053	16,477	32,953	
600	13,355	26,711	13,730	27,461	
700	11,447	22,895	11,769	23,538	
800	10,017	20,033	10,298	20,596	
900	8,904	17,807	9,154	18,307	
1000	8,013	16,026	8,238	16,477	
1100	7,285	14,569	7,489	14,979	
1200	6,678	13,355	6,865	13,730	
1300	6,164	12,328	6,337	12,674	
1400	5,724	11,447	5,884	11,769	
1500	5,342	10,684	5,492	10,984	
1600	5,008	10,017	5,149	10,298	
1700	4,714	9,427	4,846	9,692	
1800	4,452	8,904	4,577	9,154	
1900	4,217	8,435	4,336	8,672	
2000	4,007	8,013	4,119	8,238	
3000	2,671	5,342	2,746	5,492	

	BR 451B
Vertical Load Direction	Y 18.52 2 X 82
Horizontal Load Direction	Υ

BR 451B Steel Section					
Length	Allowable \	/ertical Load	Allowable Horizo	ntal Seismic Load	
Lengin	Concantrated	Distributed	Concantrated	Distributed	
mm	kN	kN	kN	kN	
300	13,611	27,222	22,229	44,457	
400	13,611	27,222	16,671	33,343	
500	11,939	23,878	13,337	26,674	
600	9,949	19,899	11,114	22,229	
700	8,528	17,056	9,527	19,053	
800	7,462	14,924	8,336	16,671	
900	6,633	13,266	7,410	14,819	
1000	5,970	11,939	6,669	13,337	
1100	5,427	10,854	6,062	12,125	
1200	4,975	9,949	5,557	11,114	
1300	4,592	9,184	5,130	10,259	
1400	4,264	8,528	4,763	9,527	
1500	3,980	7,959	4,446	8,891	
1600	3,731	7,462	4,168	8,336	
1700	3,512	7,023	3,923	7,845	
1800	3,316	6,633	3,705	7,410	
1900	3,142	6,284	3,510	7,020	
2000	2,985	5,970	3,334	6,669	
3000	1,990	3,980	2,223	4,446	



	BR 452B Steel Section				
Length		/ertical Load	Allowable Horizontal Seismic Load		
Lengin	Concantrated	Distributed	Concantrated	Distributed	
mm	kN	kN	kN	kN	
300	13,611	27,222	20,491	40,983	
400	10,920	21,840	15,369	30,737	
500	8,736	17,472	12,295	24,590	
600	7,280	14,560	10,246	20,491	
700	6,240	12,480	8,782	17,564	
800	5,460	10,920	7,684	15,369	
900	4,853	9,707	6,830	13,661	
1000	4,368	8,736	6,147	12,295	
1100	3,971	7,942	5,589	11,177	
1200	3,640	7,280	5,123	10,246	
1300	3,360	6,720	4,729	9,458	
1400	3,120	6,240	4,391	8,782	
1500	2,912	5,824	4,098	8,197	
1600	2,730	5,460	3,842	7,684	
1700	2,569	5,139	3,616	7,232	
1800	2,427	4,853	3,415	6,830	
1900	2,299	4,598	3,235	6,471	
2000	2,184	4,368	3,074	6,147	
3000	1,456	2,912	2,049	4,098	





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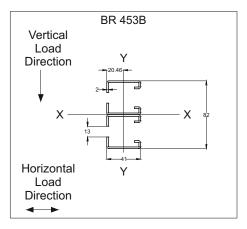
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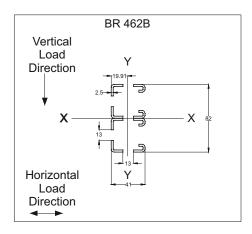
# STEP 6



	BR 453B Steel Section				
Longth	Allowable \	/ertical Load	Allowable Horizontal Seismic Load		
Length	Concentrated	Distributed	Concentrated	Distributed	
mm	kN	kN	kN	kN	
300	13,611	27,222	20,819	41,638	
400	13,611	27,222	15,614	31,229	
500	11,255	22,510	12,491	24,983	
600	9,379	18,759	10,410	20,819	
700	8,039	16,079	8,922	17,845	
800	7,035	14,069	7,807	15,614	
900	6,253	12,506	6,940	13,879	
1000	5,628	11,255	6,246	12,491	
1100	5,116	10,232	5,678	11,356	
1200	4,690	9,379	5,205	10,410	
1300	4,329	8,658	4,804	9,609	
1400	4,020	8,039	4,461	8,922	
1500	3,752	7,503	4,164	8,328	
1600	3,517	7,035	3,904	7,807	
1700	3,310	6,621	3,674	7,348	
1800	3,126	6,253	3,470	6,940	
1900	2,962	5,924	3,287	6,574	
2000	2,814	5,628	3,123	6,246	
3000	1,876	3,752	2,082	4,164	

	BR 461B
Vertical Load Direction	Y 2.5 X 52
Horizontal Load Direction	Y

	BR 461B Steel Section			
Length	Allowable \	/ertical Load	Allowable Horizontal Seismic Load	
Length	Concentrated	Distributed	Concentrated	Distributed
mm	kN	kN	kN	kN
300	16,450	32,900	27,198	54,396
400	16,450	32,900	20,399	40,797
500	14,741	29,482	16,319	32,638
600	12,284	24,568	13,599	27,198
700	10,529	21,058	11,656	23,313
800	9,213	18,426	10,199	20,399
900	8,189	16,379	9,066	18,132
1000	7,370	14,741	8,159	16,319
1100	6,700	13,401	7,418	14,835
1200	6,142	12,284	6,800	13,599
1300	5,670	11,339	6,276	12,553
1400	5,265	10,529	5,828	11,656
1500	4,914	9,827	5,440	10,879
1600	4,607	9,213	5,100	10,199
1700	4,336	8,671	4,800	9,599
1800	4,095	8,189	4,533	9,066
1900	3,879	7,758	4,294	8,589
2000	3,685	7,370	4,080	8,159
3000	2,457	4,914	2,720	5,440



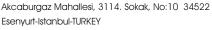
	BR 462B Steel Section			
Length	Allowable \	Allowable Vertical Load		ntal Seismic Load
Length	Concentrated	Distributed	Concentrated	Distributed
mm	kN	kN	kN	kN
300	16,450	32,900	24,912	49,825
400	13,352	26,704	18,684	37,369
500	10,682	21,363	14,947	29,895
600	8,901	17,803	12,456	24,912
700	7,630	15,259	10,677	21,353
800	6,676	13,352	9,342	18,684
900	5,934	11,868	8,304	16,608
1000	5,341	10,682	7,474	14,947
1100	4,855	9,711	6,794	13,589
1200	4,451	8,901	6,228	12,456
1300	4,108	8,217	5,749	11,498
1400	3,815	7,630	5,338	10,677
1500	3,561	7,121	4,982	9,965
1600	3,338	6,676	4,671	9,342
1700	3,142	6,283	4,396	8,793
1800	2,967	5,934	4,152	8,304
1900	2,811	5,622	3,934	7,867
2000	2,670	5,341	3,737	7,474
3000	1,780	3,561	2,491	4,982





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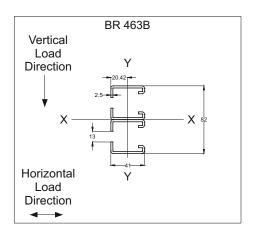
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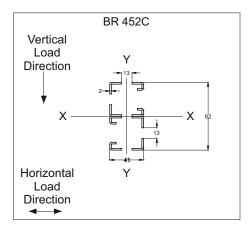
# STEP 6



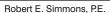
BR 463B Steel Section				
Length	Allowable Vertical Load		Allowable Horizontal Seismic Load	
Length	Concentrated	Distributed	Concentrated	Distributed
mm	kN	kN	kN	kN
300	16,450	32,900	25,398	50,796
400	16,450	32,900	19,049	38,097
500	13,866	27,733	15,239	30,478
600	11,555	23,111	12,699	25,398
700	9,905	19,809	10,885	21,770
800	8,667	17,333	9,524	19,049
900	7,704	15,407	8,466	16,932
1000	6,933	13,866	7,619	15,239
1100	6,303	12,606	6,927	13,854
1200	5,778	11,555	6,350	12,699
1300	5,333	10,666	5,861	11,722
1400	4,952	9,905	5,442	10,885
1500	4,622	9,244	5,080	10,159
1600	4,333	8,667	4,762	9,524
1700	4,078	8,157	4,482	8,964
1800	3,852	7,704	4,233	8,466
1900	3,649	7,298	4,010	8,020
2000	3,467	6,933	3,810	7,619
3000	2,311	4,622	2,540	5,080

	BR 451C
Vertical Load Direction	Υ
x —	2 X 82
Horizontal Load Direction	Υ

BR 451C Steel Section				
Length	Allowable \	Allowable Vertical Load		ntal Seismic Load
Length	Concentrated	Distributed	Concentrated	Distributed
mm	kN	kN	kN	kN
300	13,611	27,222	20,642	41,284
400	13,611	27,222	15,481	30,963
500	11,939	23,878	12,385	24,770
600	9,949	19,899	10,321	20,642
700	8,528	17,056	8,847	17,693
800	7,462	14,924	7,741	15,481
900	6,633	13,266	6,881	13,761
1000	5,970	11,939	6,193	12,385
1100	5,427	10,854	5,630	11,259
1200	4,975	9,949	5,160	10,321
1300	4,592	9,184	4,764	9,527
1400	4,264	8,528	4,423	8,847
1500	3,980	7,959	4,128	8,257
1600	3,731	7,462	3,870	7,741
1700	3,512	7,023	3,643	7,285
1800	3,316	6,633	3,440	6,881
1900	3,142	6,284	3,259	6,518
2000	2,985	5,970	3,096	6,193
3000	1,990	3,980	2,064	4,128



	BR 452C Steel Section			
Length	Allowable \	/ertical Load	Allowable Horizo	ntal Seismic Load
Length	Concentrated	Distributed	Concentrated	Distributed
mm	kN	kN	kN	kN
300	13,611	27,222	17,276	34,552
400	10,920	21,840	12,957	25,914
500	8,736	17,472	10,366	20,731
600	7,280	14,560	8,638	17,276
700	6,240	12,480	7,404	14,808
800	5,460	10,920	6,479	12,957
900	4,853	9,707	5,759	11,517
1000	4,368	8,736	5,183	10,366
1100	3,971	7,942	4,712	9,423
1200	3,640	7,280	4,319	8,638
1300	3,360	6,720	3,987	7,974
1400	3,120	6,240	3,702	7,404
1500	2,912	5,824	3,455	6,910
1600	2,730	5,460	3,239	6,479
1700	2,569	5,139	3,049	6,097
1800	2,427	4,853	2,879	5,759
1900	2,299	4,598	2,728	5,456
2000	2,184	4,368	2,591	5,183
3000	1,456	2,912	1,728	3,455





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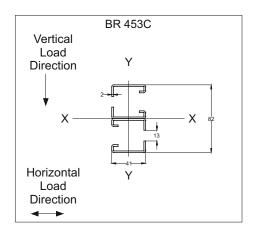
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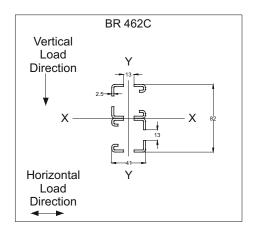
# STEP 6



BR 453C Steel Section				
Langth	Allowable V	Allowable Vertical Load		ntal Seismic Load
Length	Concentrated	Distributed	Concentrated	Distributed
mm	kN	kN	kN	kN
300	13,611	27,222	17,509	35,017
400	13,611	27,222	13,131	26,263
500	11,255	22,510	10,505	21,010
600	9,379	18,759	8,754	17,509
700	8,039	16,079	7,504	15,007
800	7,035	14,069	6,566	13,131
900	6,253	12,506	5,836	11,672
1000	5,628	11,255	5,253	10,505
1100	5,116	10,232	4,775	9,550
1200	4,690	9,379	4,377	8,754
1300	4,329	8,658	4,040	8,081
1400	4,020	8,039	3,752	7,504
1500	3,752	7,503	3,502	7,003
1600	3,517	7,035	3,283	6,566
1700	3,310	6,621	3,090	6,179
1800	3,126	6,253	2,918	5,836
1900	2,962	5,924	2,765	5,529
2000	2,814	5,628	2,626	5,253
3000	1,876	3,752	1,751	3,502

	BR 461C	
Vertical Load Direction	Y	
x —	2.5X 82	
Horizontal Load Direction	Υ	

	BR 461C Steel Section			
Length	Allowable Vertical Load		Allowable Horizontal Seismic Load	
Length	Concentrated	Distributed	Concentrated	Distributed
mm	kN	kN	kN	kN
300	16,450	32,900	25,379	50,758
400	16,450	32,900	19,034	38,069
500	14,741	29,482	15,227	30,455
600	12,284	24,568	12,690	25,379
700	10,529	21,058	10,877	21,753
800	9,213	18,426	9,517	19,034
900	8,189	16,379	8,460	16,919
1000	7,370	14,741	7,614	15,227
1100	6,700	13,401	6,922	13,843
1200	6,142	12,284	6,345	12,690
1300	5,670	11,339	5,857	11,713
1400	5,265	10,529	5,438	10,877
1500	4,914	9,827	5,076	10,152
1600	4,607	9,213	4,759	9,517
1700	4,336	8,671	4,479	8,957
1800	4,095	8,189	4,230	8,460
1900	3,879	7,758	4,007	8,014
2000	3,685	7,370	3,807	7,614
3000	2.457	4,914	2,538	5,076



BR 462C Steel Section				
Length	Allowable Vertical Load		Allowable Horizo	ntal Seismic Load
Lengin	Concentrated	Distributed	Concentrated	Distributed
mm	kN	kN	kN	kN
300	16,450	32,900	21,389	42,777
400	13,352	26,704	16,041	32,083
500	10,682	21,363	12,833	25,666
600	8,901	17,803	10,694	21,389
700	7,630	15,259	9,167	18,333
800	6,676	13,352	8,021	16,041
900	5,934	11,868	7,130	14,259
1000	5,341	10,682	6,417	12,833
1100	4,855	9,711	5,833	11,666
1200	4,451	8,901	5,347	10,694
1300	4,108	8,217	4,936	9,872
1400	3,815	7,630	4,583	9,167
1500	3,561	7,121	4,278	8,555
1600	3,338	6,676	4,010	8,021
1700	3,142	6,283	3,774	7,549
1800	2,967	5,934	3,565	7,130
1900	2,811	5,622	3,377	6,754
2000	2,670	5,341	3,208	6,417
3000	1,780	3,561	2,139	4,278

Robert E. Simmons, P.E.



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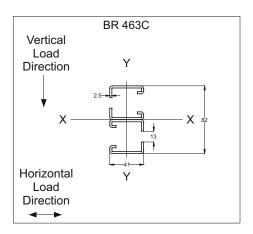
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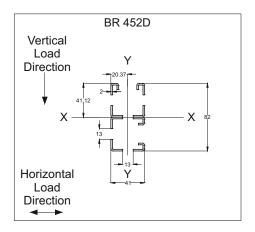
# STEP 6



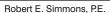
BR 463C Steel Section				
Length	Allowable V	ertical Load	Allowable Horizon	ntal Seismic Load
Lengin	Concentrated	Distributed	Concentrated	Distributed
mm	kN	kN	kN	kN
300	16,450	32,900	21,389	42,777
400	16,450	32,900	16,041	32,083
500	13,866	27,733	12,833	25,666
600	11,555	23,111	10,694	21,389
700	9,905	19,809	9,167	18,333
800	8,667	17,333	8,021	16,041
900	7,704	15,407	7,130	14,259
1000	6,933	13,866	6,417	12,833
1100	6,303	12,606	5,833	11,666
1200	5,778	11,555	5,347	10,694
1300	5,333	10,666	4,936	9,872
1400	4,952	9,905	4,583	9,167
1500	4,622	9,244	4,278	8,555
1600	4,333	8,667	4,010	8,021
1700	4,078	8,157	3,774	7,549
1800	3,852	7,704	3,565	7,130
1900	3,649	7,298	3,377	6,754
2000	3,467	6,933	3,208	6,417
3000	2,311	4,622	2,139	4,278

	BR 451D
Vertical Load Direction	Y
Horizontal Load Direction	Y

	BR 451D Steel Section				
Longth	Allowable Vertical Load		Allowable Horizontal Seismic Load		
Length	Concentrated	Distributed	Concentrated	Distributed	
mm	kN	kN	kN	kN	
300	20,417	40,834	21,615	43,230	
400	17,445	34,890	16,211	32,423	
500	13,956	27,912	12,969	25,938	
600	11,630	23,260	10,808	21,615	
700	9,969	19,937	9,264	18,527	
800	8,723	17,445	8,106	16,211	
900	7,753	15,507	7,205	14,410	
1000	6,978	13,956	6,485	12,969	
1100	6,344	12,687	5,895	11,790	
1200	5,815	11,630	5,404	10,808	
1300	5,368	10,735	4,988	9,976	
1400	4,984	9,969	4,632	9,264	
1500	4,652	9,304	4,323	8,646	
1600	4,361	8,723	4,053	8,106	
1700	4,105	8,209	3,814	7,629	
1800	3,877	7,753	3,603	7,205	
1900	3,673	7,345	3,413	6,826	
2000	3,489	6,978	3,242	6,485	
3000		4.652	2.162	4.323	



	BR 452D Steel Section				
Length	Allowable Vertical Load		Allowable Horizontal Seismic Load		
Length	Concentrated	Distributed	Concentrated	Distributed	
mm	kN	kN	kN	kN	
300	18,769	37,539	17,758	35,516	
400	14,077	28,154	13,319	26,637	
500	11,262	22,523	10,655	21,310	
600	9,385	18,769	8,879	17,758	
700	8,044	16,088	7,611	15,221	
800	7,039	14,077	6,659	13,319	
900	6,256	12,513	5,919	11,839	
1000	5,631	11,262	5,327	10,655	
1100	5,119	10,238	4,843	9,686	
1200	4,692	9,385	4,440	8,879	
1300	4,331	8,663	4,098	8,196	
1400	4,022	8,044	3,805	7,611	
1500	3,754	7,508	3,552	7,103	
1600	3,519	7,039	3,330	6,659	
1700	3,312	6,624	3,134	6,268	
1800	3,128	6,256	2,960	5,919	
1900	2,964	5,927	2,804	5,608	
2000	2,815	5,631	2,664	5,327	
3000	1,877	3,754	1,776	3,552	





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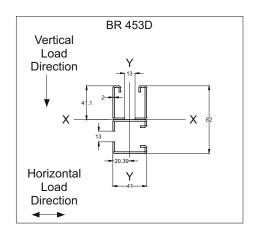
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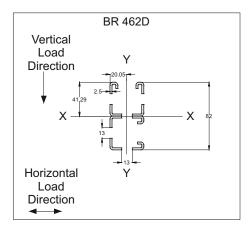
# STEP 6



	BR 453D Steel Section				
Longth	Allowable \	/ertical Load	Allowable Horizontal Seismic Load		
Length	Concentrated	Distributed	Concentrated	Distributed	
mm	kN	kN	kN	kN	
300	20,417	40,834	21,015	42,030	
400	17,285	34,570	15,761	31,523	
500	13,828	27,656	12,609	25,218	
600	11,523	23,047	10,508	21,015	
700	9,877	19,754	9,007	18,013	
800	8,643	17,285	7,881	15,761	
900	7,682	15,364	7,005	14,010	
1000	6,914	13,828	6,305	12,609	
1100	6,285	12,571	5,731	11,463	
1200	5,762	11,523	5,254	10,508	
1300	5,318	10,637	4,850	9,699	
1400	4,939	9,877	4,503	9,007	
1500	4,609	9,219	4,203	8,406	
1600	4,321	8,643	3,940	7,881	
1700	4,067	8,134	3,709	7,417	
1800	3,841	7,682	3,503	7,005	
1900	3,639	7,278	3,318	6,636	
2000	3,457	6,914	3,152	6,305	
3000	2,305	4,609	2,102	4,203	

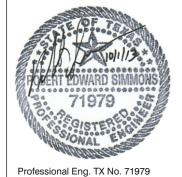
	BR 461D
Vertical Load Direction	Y 2.5 X 82
Horizontal Load Direction	Y

	BR 461D Steel Section				
Length	Allowable \	/ertical Load	Allowable Horizontal Seismic Load		
Length	Concentrated	Distributed	Concentrated	Distributed	
mm	kN	kN	kN	kN	
300	24,670	49,340	26,627	53,253	
400	21,913	43,826	19,970	39,940	
500	17,530	35,061	15,976	31,952	
600	14,609	29,217	13,313	26,627	
700	12,522	25,043	11,411	22,823	
800	10,957	21,913	9,985	19,970	
900	9,739	19,478	8,876	17,751	
1000	8,765	17,530	7,988	15,976	
1100	7,968	15,937	7,262	14,524	
1200	7,304	14,609	6,657	13,313	
1300	6,742	13,485	6,145	12,289	
1400	6,261	12,522	5,706	11,411	
1500	5,843	11,687	5,325	10,651	
1600	5,478	10,957	4,993	9,985	
1700	5,156	10,312	4,699	9,398	
1800	4,870	9,739	4,438	8,876	
1900	4,613	9,227	4,204	8,408	
2000	4,383	8,765	3,994	7,988	
3000	2,922	5,843	2,663	5,325	



	BR 462D Steel Section				
Length	Allowable Vertical Load		Allowable Horizontal Seismic Load		
Lengui	Concentrated	Distributed	Concentrated	Distributed	
mm	kN	kN	kN	kN	
300	23,327	46,653	21,693	43,387	
400	17,495	34,990	16,270	32,540	
500	13,996	27,992	13,016	26,032	
600	11,663	23,327	10,847	21,693	
700	9,997	19,994	9,297	18,594	
800	8,748	17,495	8,135	16,270	
900	7,776	15,551	7,231	14,462	
1000	6,998	13,996	6,508	13,016	
1100	6,362	12,724	5,916	11,833	
1200	5,832	11,663	5,423	10,847	
1300	5,383	10,766	5,006	10,012	
1400	4,999	9,997	4,649	9,297	
1500	4,665	9,331	4,339	8,677	
1600	4,374	8,748	4,068	8,135	
1700	4,116	8,233	3,828	7,656	
1800	3,888	7,776	3,616	7,231	
1900	3,683	7,366	3,425	6,851	
2000	3,499	6,998	3,254	6,508	
3000	2,333	4,665	2,169	4,339	





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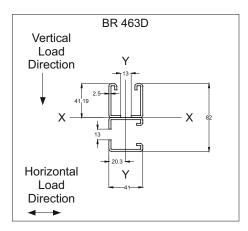
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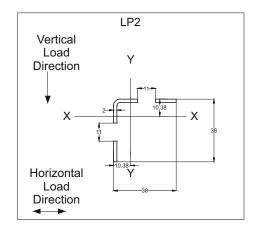
# STEP 6



	BR 463D Steel Section				
1	Allowable \	/ertical Load	Allowable Horizon	ntal Seismic Load	
Length	Concentrated	Distributed	Concentrated	Distributed	
mm	kN	kN	kN	kN	
300	24,670	49,340	25,851	51,703	
400	21,686	43,372	19,389	38,777	
500	17,349	34,698	15,511	31,022	
600	14,457	28,915	12,926	25,851	
700	12,392	24,784	11,079	22,158	
800	10,843	21,686	9,694	19,389	
900	9,638	19,276	8,617	17,234	
1000	8,674	17,349	7,755	15,511	
1100	7,886	15,772	7,050	14,101	
1200	7,229	14,457	6,463	12,926	
1300	6,673	13,345	5,966	11,931	
1400	6,196	12,392	5,540	11,079	
1500	5,783	11,566	5,170	10,341	
1600	5,422	10,843	4,847	9,694	
1700	5,103	10,205	4,562	9,124	
1800	4,819	9,638	4,309	8,617	
1900	4,565	9,131	4,082	8,164	
2000	4,337	8,674	3,878	7,755	
3000	2,891	5,783	2,585	5,170	

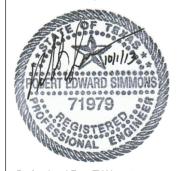
	AT4
Vertical Load Direction	Y 7.5 X 33
Horizontal Load Direction	Υ

	AT4 Steel Section				
Length	Allowable \	/ertical Load	Allowable Horizontal Seismic Load		
Length	Concentrated	Distributed	Concentrated	Distributed	
mm	kN	kN	kN	kN	
300	1,851	3,702	0,954	1,908	
400	1,388	2,776	0,715	1,431	
500	1,111	2,221	0,572	1,145	
600	0,925	1,851	0,477	0,954	
700	0,793	1,587	0,409	0,818	
800	0,694	1,388	0,358	0,715	
900	0,617	1,234	0,318	0,636	
1000	0,555	1,111	0,286	0,572	
1100	0,505	1,010	0,260	0,520	
1200	0,463	0,925	0,238	0,477	
1300	0,427	0,854	0,220	0,440	
1400	0,397	0,793	0,204	0,409	
1500	0,370	0,740	0,191	0,382	
1600	0,347	0,694	0,179	0,358	
1700	0,327	0,653	0,168	0,337	
1800	0,308	0,617	0,159	0,318	
1900	0,292	0,585	0,151	0,301	
2000	0,278	0,555	0,143	0,286	
3000	0,185	0,370	0,095	0,191	



	LP2 Steel Section			
Length	Allowable Vertical Load		Allowable Horizontal Seismic Load	
Length	Concentrated	Distributed	Concentrated	Distributed
mm	kN	kN	kN	kN
300	0,902	1,804	1,288	2,577
400	0,676	1,353	0,966	1,933
500	0,541	1,082	0,773	1,546
600	0,451	0,902	0,644	1,288
700	0,387	0,773	0,552	1,104
800	0,338	0,676	0,483	0,966
900	0,301	0,601	0,429	0,859
1000	0,271	0,541	0,387	0,773
1100	0,246	0,492	0,351	0,703
1200	0,225	0,451	0,322	0,644
1300	0,208	0,416	0,297	0,595
1400	0,193	0,387	0,276	0,552
1500	0,180	0,361	0,258	0,515
1600	0,169	0,338	0,242	0,483
1700	0,159	0,318	0,227	0,455
1800	0,150	0,301	0,215	0,429
1900	0,142	0,285	0,203	0,407
2000	0,135	0,271	0,193	0,387
3000	0,090	0,180	0,129	0,258





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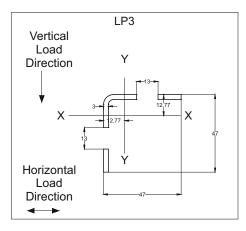
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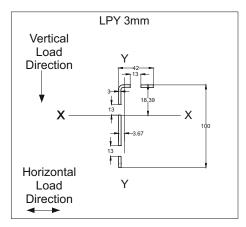
# STEP 6



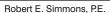
	LP3 Steel Section				
Langth	Allowable V	/ertical Load	Allowable Horizontal Seismic Loa		
Length	Concentrated	Distributed	Concentrated	Distributed	
mm	kN	kN	kN	kN	
300	2,685	5,370	3,836	7,672	
400	2,014	4,028	2,877	5,754	
500	1,611	3,222	2,301	4,603	
600	1,343	2,685	1,918	3,836	
700	1,151	2,301	1,644	3,288	
800	1,007	2,014	1,438	2,877	
900	0,895	1,790	1,279	2,557	
1000	0,806	1,611	1,151	2,301	
1100	0,732	1,465	1,046	2,092	
1200	0,671	1,343	0,959	1,918	
1300	0,620	1,239	0,885	1,770	
1400	0,575	1,151	0,822	1,644	
1500	0,537	1,074	0,767	1,534	
1600	0,503	1,007	0,719	1,438	
1700	0,474	0,948	0,677	1,354	
1800	0,448	0,895	0,639	1,279	
1900	0,424	0,848	0,606	1,211	
2000	0,403	0,806	0,575	1,151	
3000	0,269	0,537	0,384	0,767	

	LP4
Vertical Load Direction	Υ
X —	4-13-1331 X
Horizontal Load Direction	47

LP4 Steel Section				
Length	Allowable Vertical Load		Allowable Horizontal Seismic L	
Lengin	Concentrated	Distributed	Concentrated	Distributed
mm	kN	kN	kN	kN
300	3,509	7,017	5,012	10,024
400	2,631	5,263	3,759	7,518
500	2,105	4,210	3,007	6,015
600	1,754	3,509	2,506	5,012
700	1,504	3,007	2,148	4,296
800	1,316	2,631	1,880	3,759
900	1,170	2,339	1,671	3,341
1000	1,053	2,105	1,504	3,007
1100	0,957	1,914	1,367	2,734
1200	0,877	1,754	1,253	2,506
1300	0,810	1,619	1,157	2,313
1400	0,752	1,504	1,074	2,148
1500	0,702	1,403	1,002	2,005
1600	0,658	1,316	0,940	1,880
1700	0,619	1,238	0,885	1,769
1800	0,585	1,170	0,835	1,671
1900	0,554	1,108	0,791	1,583
2000	0,526	1,053	0,752	1,504
3000	0,351	0,702	0,501	1,002



LPY-3mm Steel Section				
Length	Allowable Verti		Allowable Horizo	ntel Seismic Load
Length	Concentrated	Distributed	Concentrated	Distributed
mm	kN	kN	kN	kN
300	6,618	13,237	3,194	6,388
400	4,964	9,928	2,396	4,791
500	3,971	7,942	1,916	3,833
600	3,309	6,618	1,597	3,194
700	2,836	5,673	1,369	2,738
800	2,482	4,964	1,198	2,396
900	2,206	4,412	1,065	2,129
1000	1,986	3,971	0,958	1,916
1100	1,805	3,610	0,871	1,742
1200	1,655	3,309	0,799	1,597
1300	1,527	3,055	0,737	1,474
1400	1,418	2,836	0,684	1,369
1500	1,324	2,647	0,639	1,278
1600	1,241	2,482	0,599	1,198
1700	1,168	2,336	0,564	1,127
1800	1,103	2,206	0,532	1,065
1900	1,045	2,090	0,504	1,009
2000	0,993	1,986	0,479	0,958
3000	0,662	1,324	0,319	0,639





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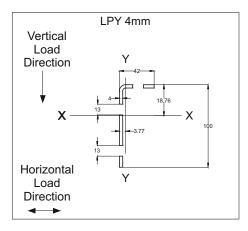
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	LPY-4mm Steel Section				
Longth	Allowable Vertical Load		Allowable Horizontel Seismic Load		
Length	Concentrated	Distributed	Concentrated	Distributed	
mm	kN	kN	kN	kN	
300	12,844	25,687	4,184	8,368	
400	9,633	19,265	3,138	6,276	
500	7,706	15,412	2,511	5,021	
600	6,422	12,844	2,092	4,184	
700	5,504	11,009	1,793	3,586	
800	4,816	9,633	1,569	3,138	
900	4,281	8,562	1,395	2,789	
1000	3,853	7,706	1,255	2,511	
1100	3,503	7,006	1,141	2,282	
1200	3,211	6,422	1,046	2,092	
1300	2,964	5,928	0,966	1,931	
1400	2,752	5,504	0,897	1,793	
1500	2,569	5,137	0,837	1,674	
1600	2,408	4,816	0,785	1,569	
1700	2,267	4,533	0,738	1,477	
1800	2,141	4,281	0,697	1,395	
1900	2,028	4,056	0,661	1,321	
2000	1,927	3,853	0,628	1,255	
3000	1,284	2,569	0,418	0,837	

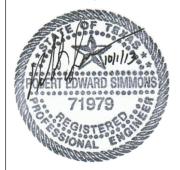
	ZPY 3mm
Vertical Load Direction	Y  -42  -13
Horizontal Load Direction	Υ

	ZPY-3mm Steel Section				
Length	Allowable Vertical Load		Allowable Horizontel Seismic Loa		
Lengui	Concentrated	Distributed	Concentrated	Distributed	
mm	kN	kN	kN	kN	
300	11,284	22,569	6,549	13,099	
400	8,463	16,927	4,912	9,824	
500	6,771	13,541	3,930	7,859	
600	5,642	11,284	3,275	6,549	
700	4,836	9,672	2,807	5,614	
800	4,232	8,463	2,456	4,912	
900	3,761	7,523	2,183	4,366	
1000	3,385	6,771	1,965	3,930	
1100	3,078	6,155	1,786	3,572	
1200	2,821	5,642	1,637	3,275	
1300	2,604	5,208	1,511	3,023	
1400	2,418	4,836	1,403	2,807	
1500	2,257	4,514	1,310	2,620	
1600	2,116	4,232	1,228	2,456	
1700	1,991	3,983	1,156	2,312	
1800	1,881	3,761	1,092	2,183	
1900	1,782	3,563	1,034	2,068	
2000	1,693	3,385	0,982	1,965	
3000	1,128	2,257	0,655	1,310	

	ZPY 4mm
Vertical Load Direction	Y 42 13 4 X 64
Horizontal Load Direction	Υ

	ZPY-4mm Steel Section				
Length	Allowable Vertical Load		Allowable Horizontel Seismic Loa		
Length	Concentrated	Distributed	Concentrated	Distributed	
mm	kN	kN	kN	kN	
300	14,012	28,024	8,558	17,116	
400	10,509	21,018	6,419	12,837	
500	8,407	16,814	5,135	10,270	
600	7,006	14,012	4,279	8,558	
700	6,005	12,010	3,668	7,336	
800	5,255	10,509	3,209	6,419	
900	4,671	9,341	2,853	5,705	
1000	4,204	8,407	2,567	5,135	
1100	3,821	7,643	2,334	4,668	
1200	3,503	7,006	2,140	4,279	
1300	3,234	6,467	1,975	3,950	
1400	3,003	6,005	1,834	3,668	
1500	2,802	5,605	1,712	3,423	
1600	2,627	5,255	1,605	3,209	
1700	2,473	4,945	1,510	3,021	
1800	2,335	4,671	1,426	2,853	
1900	2,212	4,425	1,351	2,703	
2000	2,102	4,204	1,284	2,567	
3000	1,401	2,802	0,856	1,712	





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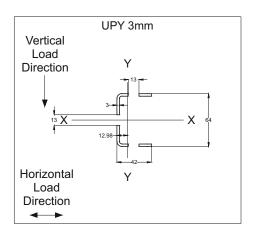
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# STEP 6



UPY-3mm Steel Section				
Length	Allowable Vertical Load		Allowable Horizontal Seismic Loa	
Length	Concentrated	Distributed	Concentrated	Distributed
mm	kN	kN	kN	kN
300	12,941	25,883	5,835	11,670
400	9,706	19,412	4,376	8,753
500	7,765	15,530	3,501	7,002
600	6,471	12,941	2,918	5,835
700	5,546	11,093	2,501	5,001
800	4,853	9,706	2,188	4,376
900	4,314	8,628	1,945	3,890
1000	3,882	7,765	1,751	3,501
1100	3,529	7,059	1,591	3,183
1200	3,235	6,471	1,459	2,918
1300	2,986	5,973	1,347	2,693
1400	2,773	5,546	1,250	2,501
1500	2,588	5,177	1,167	2,334
1600	2,427	4,853	1,094	2,188
1700	2,284	4,568	1,030	2,059
1800	2,157	4,314	0,973	1,945
1900	2,043	4,087	0,921	1,843
2000	1,941	3,882	0,875	1,751
3000	1,294	2,588	0,584	1,167

	UPY 4mm
Vertical Load Direction	Y 13.51 13.51 X 64
Horizontal Load Direction	Y

	UPY-4mm Steel Section					
Length	Allowable \	/ertical Load	Allowable Horizon	ntal Seismic Load		
Lengin	Concentrated	Distributed	Concentrated	Distributed		
mm	kN	kN	kN	kN		
300	17,427	34,853	7,600	15,200		
400	13,070	26,140	5,700	11,400		
500	10,456	20,912	4,560	9,120		
600	8,713	17,427	3,800	7,600		
700	7,469	14,937	3,257	6,514		
800	6,535	13,070	2,850	5,700		
900	5,809	11,618	2,533	5,067		
1000	5,228	10,456	2,280	4,560		
1100	4,753	9,505	2,073	4,145		
1200	4,357	8,713	1,900	3,800		
1300	4,022	8,043	1,754	3,508		
1400	3,734	7,469	1,629	3,257		
1500	3,485	6,971	1,520	3,040		
1600	3,268	6,535	1,425	2,850		
1700	3,075	6,151	1,341	2,682		
1800	2,904	5,809	1,267	2,533		
1900	2,752	5,503	1,200	2,400		
2000	2,614	5,228	1,140	2,280		
3000	1,743	3,485	0,760	1,520		





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## STEP 7

### **Determining Rod**

Tensional loading of trapeze rods should be determined by following calculation:

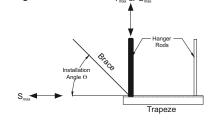
$$T_{\text{max}} = \left[ \frac{D + 0.7F_{\text{V}}}{2} + (F_{\text{Ptmax}} \times 0.7 \times \tan \Theta) \right]$$

Compression loading of trapeze rods should be determined by following calculation:

$$C_{\text{max}} = \left[ \frac{D-0.7F}{2} - (F_{\text{Ptmax}} \times 0.7 \times \tan \Theta) \right]$$

Shear load of trapeze rods should be determined by following calculation:

$$S_{max} = F_{Ptmax} \times 0.7$$



 $\Gamma_{\text{max}}$ : Maximum rod tension.  $C_{\text{max}}$ : Maximum rod compression.

 $S_{\text{max}}$ : Maximum rod shear.

Component operating weight (operating vertical load, dead load).

 $F_{\mbox{\tiny Ptmax}}$ : Maximum transverse (lateral) seismic design force.

 $F_v$ : Vertical sysmic design force.  $tan\Theta$ : Tangent of installation angle.

Rod Size	Allowable Tension Load	Allowable Compression Load I/r <200	Allowable Seismic Load tension or compression	
mm	kN	kN	kN	kN
M8	1.64	0.83	2.18	10.4
M10	2.6	1.11	3.45	16.26
M12	3.8	1.58	5.05	23.11

Combined loads should satisfy below calculation:

$$\frac{T_{\text{max}} \text{ or } C_{\text{max}}}{\text{Allowable seismic load}} + \frac{S_{\text{max}}}{\text{Allowable shear load}} \leqslant 1$$

#### Example 6:

Installation angle for system described in example 5 is 45 degrees. Rod loads are:

 $T_{max} = [(1.015+0.7x0.224)/2+(4.518x0.7x1)] = 3.748 \text{ kN's}.$ 

 $C_{max} = [(1.015-0.7x0.224)/2-(4.518x0.7x1)] = -2.74 \text{ kN's}$ , compression exists.

 $S_{max} = 4.518 \times 0.7 = 3.163 \text{ kN/s}.$ 

 $\frac{3.748}{5.05} + \frac{3.163}{23.11} = 0.88 < 1$ , M12 Rod is ok.





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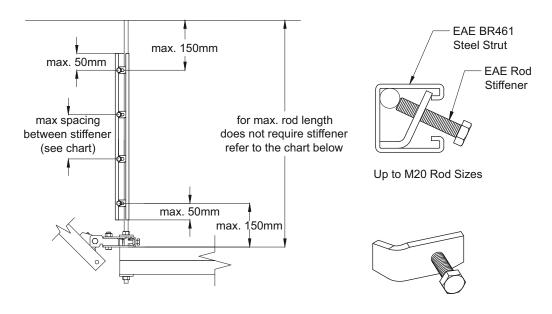
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## STEP 8

## **Determining Rod Stiffener**

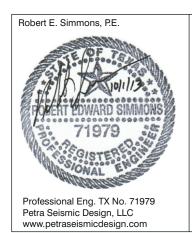
If threaded rod length exceed the values of table below, rod stiffeners should be used in order to prevent rod from buckling.



Rod Size	Max. Rod Length Without Stiffener	Max. Spacing Between Stiffener
M 8	300 mm	225 mm
M 10	475 mm	325 mm
M 12	625 mm	450 mm
M 16	775 mm	575 mm
M 20	925 mm	700 mm

Rod stiffeners are required only on hanger and trapeze assemblies that have seismic bracing attached at or within 100mm of the rod. A minimum of two stiffeners must be installed.

<sup>\*</sup>Recommended Torque is 10.8 Nm (or finger tight plus one full turn with a wrench).



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## STEP 9

## **Determining Brace Installation**

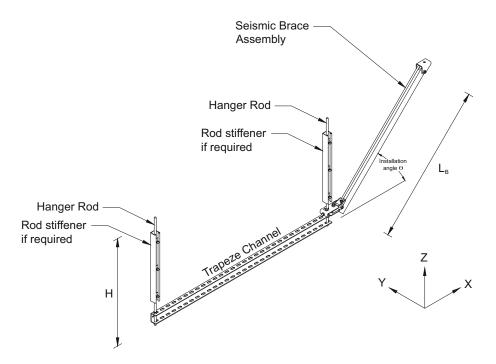
In order to determine brace installation, following values must be specified.

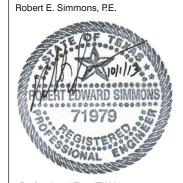
 $L_{\scriptscriptstyle B}$ : Brace section length must be determined. In case of brace and rod anchored to ceiling, brace length can be calculated by the total rod length (H) divided by cosine of the installation angle( $\Theta$ ).

If brace is planning to be attached other than ceiling keep in mind;

- Brace should be attached to a structural component.
- Do not attach brace to a different structural component than trapeze assembly. ie. ceiling and wall.
- In case of brace attached to wall, proper wall anchorage should be done by using right anchors.
- In case of brace attached to a steel beam, right attachment tool should be provided. Refer step 12 for steel beam attachments.

Installation angle should also be provided. Optimum installation angle is 45°, but the design of the brace permits 35° to 70° of installation angle.





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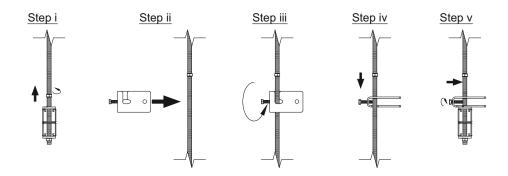


## STEP 9

## **Determining Brace Installation**

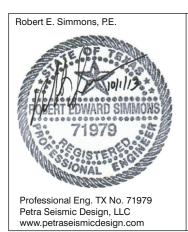
Installation Instructions for seismic brace assembly:

Stage I: Preperation of threaded rod retrofit fixing



Stage II: Preperation of brace section





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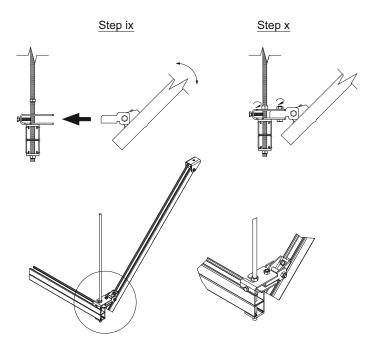


## STEP 9

### **Determining Brace Installation**

Installation Instructions for seismic brace assembly continue:

Stage III: Fastening brace to trapeze assembly



### Stage I:

unfasten trapeze nut, place retrofit fixing to trapeze rod and rotate until it faces down. Fasten rod screw on retrofit fixing (recommended torque 20 Nm).

### Stage II:

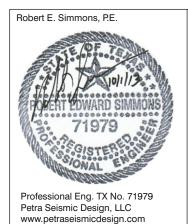
Place spring nut into brace channel. Place brace joint into brace channel. Set brace length before fastening. Fasten secure head-off bolt until its head brakes off, than fasten nut (recommended torque 20 Nm).

#### Stage III:

Place brace into retrofit fixing. Adjust installation angle. Fasten retrofit fixing to brace and fasten trapeze nut (recommended torque 20 Nm).

#### Notes

For anchorage see section 12



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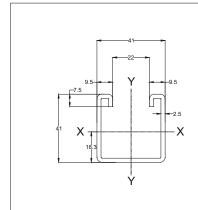




## **STEP 10**

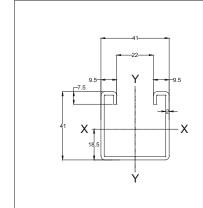
## **Determining Brace Section**

Once brace length and installation angle is determined, brace section should be selected following tables. Use round up values for brace length and installation angle. If section strength is not enough for seismic forces, decrease maximum brace spacing  $S_{\scriptscriptstyle B}$  and therefor  $F_{\scriptscriptstyle D}$  horizontal seismic design force.



#### **BR461 Channel**

Unsupported	Max. Allowable		
Length	Compression Load		
mm	kN		
1500	12.61		
2000	9.20		
2500	7.07		
3000	5.53		
3500	4.51		
4000	3.57		
4500	2.81		
5000	2.23		
5500	1.87		
6000	1.53		

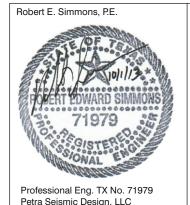


#### **BR451 Channel**

Unsupported	Max. Allowable		
Length	Compression Load		
mm	kN		
1500	8.43		
2000	6.13		
2500	4.77		
3000	3.83		
3500	3.15		
4000	2.64		
4500	2.21		
5000	1.87		
5500	1.61		
6000	1.27		
-			

### Notes:

The allowable compression loads are calculated according to AISI 1996 allowable stress design (ASD) and the material used is DIN10025-P2 S235JR.



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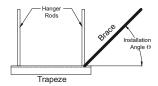
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# **STEP 10**

## **Determining Brace Section**



**BR461 Channel** 

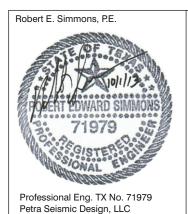
Length of the Channel used in the Brace	max. Allowable Horizontal Seismic Load (F <sub>P</sub> ) at max. Compressive load		
Assembly (L <sub>R</sub> )	45±10° 60±10°		
	installation angle θ	installation angle $\Theta$	
mm	kN	kN	
1500	10.33	6.16	
2000	7.54	4.49	
2500	5.79	3.45	
3000	4.53	2.70	
3500	3.70	2.20	
4000	2.92	1.74	
4500	2.31	1.38	
5000	1.82	1.09	
5500	1.53	0.92	
6000	1.25	0.75	

**BR451 Channel** 

Length of the Channel used in the Brace	max. Allowable Horizontal Seismic Load (F <sub>p</sub> ) at max. Compressive load		
Assembly (L <sub>B</sub> )	45±10° 60±10°		
	installation angle $\Theta$	installation angle $\Theta$	
mm	kN	kN	
1500	6.91	4.12	
2000	5.02	2.99	
2500	3.91	2.33	
3000	3.14	1.87	
3500	2.58	1.54	
4000	2.16	1.29	
4500	1.81	1.08	
5000	1.53	0.92	
5500	1.32	0.79	
6000	1.04	0.62	

#### Notes:

The allowable horizontal seismic loads given are according ASCE/SEI 7.10 2.4.1 ASD combination 5 (D+0.7E).



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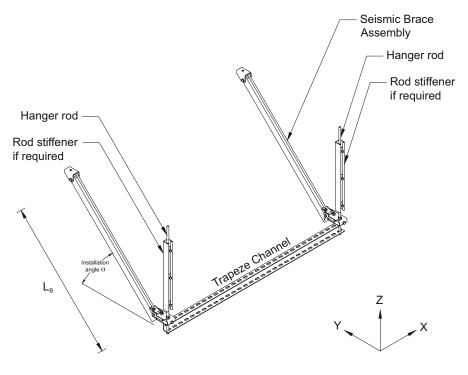
# **STEP 10**

## **Determining Brace Section**

### Example 7:

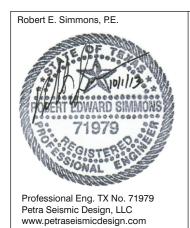
Lateral and longitudinal brace sections of example 6 are being determined.  $L_{\scriptscriptstyle B}$  of the brace section is 1500mm and installation angle ( $\Theta$ ) is 45±10°. Brace section should be able to resist:

### Longitudinal:



Brace section load =  $F_{Pimax}/2$ 

= 6.024/2 = 3.013 kN/s.



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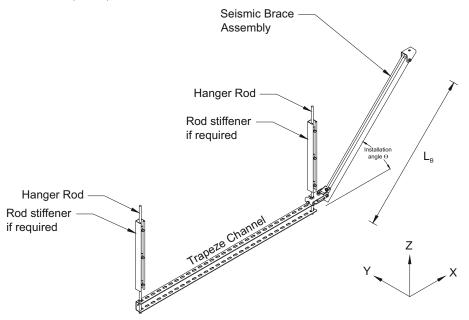


# **STEP 10**

### **Determining Brace Section**

Example 7 continue:

Transverse (lateral):



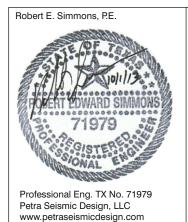
Brace section load = F<sub>Ptmax</sub>

4.518 kN's.

3.013 kN<6.91 kN for longitudinal brace, BR451 section is ok.
4.518 kN<6.91 kN for transverse (lateral) brace, BR451 section is ok.

Notes:

Refer to page A4-1 to A4-3 for  $F_{Plmax}$  and  $F_{Plmax}$ .



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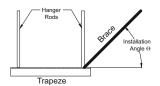




# **STEP 11**

## **Determining Anchor Loads**

Anchor load values with prying factors at maximum allowable loads are given in the tables below. Interpolation can be done to reach actual load values.

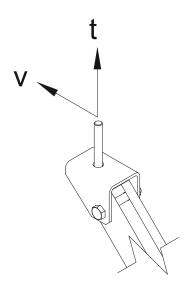


**BR461 Channel** 

Length of the Channel used in the Brace Assembly	Anchor Reactions under max. Allowable Loads with Prying Factor			
	45±10°		60±10°	
Accountry	installation angle θ		installation angle θ	
	t	V	t	V
mm	kN	kN	kN	kN
1500	8.45	7.23	17.54	4.31
2000	6.17	5.28	12.79	3.15
2500	4.74	4.06	9.83	2.42
3000	3.71	3.17	7.69	1.89
3500	3.02	2.59	6.27	1.54
4000	2.39	2.05	4.96	1.22
4500	1.89	1.61	3.91	0.96
5000	1.49	1.28	3.10	0.76
5500	1.26	1.07	2.60	0.64
6000	1.03	0.88	2.13	0.52



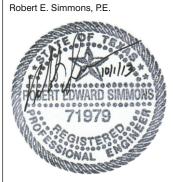
Length of the Channel	Anchor Reactions under max. Allowable Loads with Prying Factor			
used in the Brace	used in the Brace 45±10		60	±10°
Assembly	installation angle $\Theta$		installation angle $\Theta$	
	t	V	t	V
mm	kN	kN	kN	kN
1500	5.65	4.84	11.73	2.88
2000	4.11	3.52	8.52	2.10
2500	3.19	2.73	6.63	1.63
3000	2.57	2.20	5.33	1.31
3500	2.11	1.81	4.38	1.08
4000	1.77	1.51	3.67	0.90
4500	1.48	1.27	3.07	0.75
5000	1.26	1.07	2.60	0.64
5500	1.08	0.92	2.24	0.55
6000	0.85	0.73	1.76	0.43



- t: Anchor tension
- v: Anchor shear

### Notes:

Values given in the tables are for installations parallel to trapeze level like ceiling. The prying factor is changing with installation angle. Consult with a design professional for more information.



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## **STEP 11**

## **Determining Anchor Loads**

#### Example 8:

To Determine brace anchor reactions in example 7, following interpolation should be done:

Load percentage = Brace section load / max. Allowable brace section load x 100

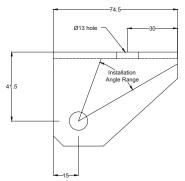
Load percentage = 4.518/6.91x100 = 66% for transverse (lateral) brace.

Actual anchor reaction = load percentage x Reaction at max. allowable loads

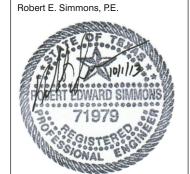
t = 0.66x5.65 = 3.73 kN's for lateral brace. v = 0.66x4.84 = 3.20 kN's for lateral brace.

Load percentage = 3.013/6.91x100 = 44% for longitudinal brace.

t = 0.44x5.65 = 2.49 kN's for longitudinal brace. v = 0.44x4.84 = 2.13 kN's for longitudinal brace.



**Brace Ceiling Attachment Piece** 



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## **STEP 12**

### **Determining Brace Anchor**

Once anchor reactions determined, concrete anchor selection and calculations should be done according to ACI-318 appendix D. Provided min. edge distance, min. slab quality and thickness is present, single concrete anchor installations should meet following condition:

$$\left(\frac{t}{T_{ASDallow}}\right)^{5/3} + \left(\frac{v}{V_{ASDallow}}\right)^{5/3} < 1$$

#### Example 9:

The concrete anchor decided to fasten brace to ceiling has following properties:

 $T_{ASD,allow}$  = 10.67 kN  $V_{ASD,allow}$  = 23.6 kN

Combined load calculation of the brace anchor in example 8 should be done:

 $(3.73/10.67)^{(5/3)} + (3.20/23.6)^{(5/3)} = 0.21 < 1$  lateral anchorage is ok.

 $(2.49/10.67)^{(5/3)} + (2.13/23.6)^{(5/3)} = 0.11 < 1$  longitudinal anchorage is ok.

#### Notes:

Installation instructions of anchor manufacturer should be followed. Post-installed concrete anchors should be prequalified for seismic applications in accordance with ACI 355.2 or manufacturer should approve anchor should withstand anchor loads by other equivalent sources like ETAG. In cases where single anchor does not meet the load criteria above, use UDY 150 anchor assembly in order to increase anchor quantity. Group anchor calculations should be done in accordance with ACI 318 appendix D or manufacturer should approve anchors should withstand anchor loads by other equivalent sources like ETAG. For more information on post-installed concrete anchors, consult with manufacturer design professional.

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## **STEP 12**

## **Determining Brace Anchor**

Generic expansion anchor allowable loads are given below for consideration.

Expansion Anchor Tension and Shear Values (3000 psi normal weight concrete slab)

Anchor Diameter	Anchor Embedment	Minimum Slab Thickness	Minimum Edge Distance	Allowable Tension	Allowable Shear		
in - mm	in - mm	in - mm	in - <i>mm</i>	lb - <i>kN</i>	lb - <i>kN</i>		
2/9 1/40	<b>2</b> - 102	<b>4</b> - 102	<b>6</b> - 152	<b>485</b> - 2.16	<b>710</b> - 3.16		
<b>3/8</b> - <i>M</i> 10	<b>2 7/8</b> - 127	<b>5</b> - 127	<b>6</b> - 152	<b>1035</b> - <i>4.60</i>	<b>820</b> - 3.65		
<b>1/2</b> - <i>M</i> 12	<b>2 3/4</b> - 127	<b>5</b> - 127	<b>6</b> - 152	<b>1070</b> - <i>4.</i> 76	<b>1055</b> - 4.69		
112 - 1/112	<b>3 7/8</b> - 152	<b>6</b> - 152	<b>8</b> - 203	<b>1395</b> - 6.21	<b>2100</b> - 9.34		
<b>5/8</b> - <i>M</i> 16	<b>3 3/8</b> - 203	<b>6</b> - 203	<b>8</b> - 203	<b>1450</b> - 6.45	<b>2155</b> - 9.59		
3/6 - W//O	<b>5 1/8</b> - 203	<b>8</b> - 203	<b>8</b> - 203	<b>2575</b> - 11.45	<b>2750</b> - 12.23		
3/4 - M20	<b>4 1/8</b> - 203	<b>8</b> - 203	<b>10</b> - 229	<b>1665</b> - 7.41	<b>3425</b> - 15.24		
314 - 1/120	<b>5 3/4</b> - 229	<b>9</b> - 229	<b>10</b> - 229	<b>3005</b> - <i>13.37</i>	<b>3930</b> - <i>17.48</i>		
1 - M24	<b>5 1/4</b> - 229	<b>9</b> - 229	<b>10</b> - 229	<b>2435</b> - 10.83	<b>4195</b> - <i>18.66</i>		

#### Notes:

- 1. Values in table are for single anchors only and not valid for anchors installed in groups.
- 2. Each anchor is considered to be in the corner of slab with the minimum edge distance present on two sides.
- 3. Values are for ASD Seismic loads in cracked concrete for nonstructural component attachments.
- 4. Calculations assume supplementary reinforcement Condition B and minimum #4 bar between the anchor and edge of the slab.
- 5. Values used for anchor design must be determined using ACI 318 Appendix D in conjunction with appropriate ICC ES Report.

## Expansion Anchor Tension And Shear Values (Underside of 3000 psi lightweight-comcrete-filled metal deck)

Anchor Diameter	Anchor Embedment	Minimum Spacing	Allowable Tension	Allowable Shear		
in - mm	in - mm	in - mm	lb - <i>kN</i>	lb - <i>kN</i>		
<b>3/8</b> - <i>M</i> 10	<b>3 3/8</b> - 86	<b>9</b> - 229	<b>761</b> - 3.39	<b>1588</b> - 7.06		
<b>1/2</b> - <i>M</i> 12	<b>4 1/2</b> - 114	<b>12</b> - 305	<b>932</b> - 4.15	<b>2084</b> - 9.27		
<b>5/8</b> - <i>M</i> 16	<b>4 5/8</b> - 117	<b>12</b> - 305	<b>1342</b> - 5.97	<b>2302</b> - 10.24		

#### Notes:

- 1. Minimum 20 gage profile metal deck with min. 4 1/2 in. (114mm) wide x maximm 3 in. (76 mm) deep flutes.
- 2. Anchors installed in the lower flute with up to 1 in. (25 mm) offset from center.
- 3. Values used for anchor design must be determined using ACI 318 Appendix D in conjunction with the appropriate ICC ES Report.

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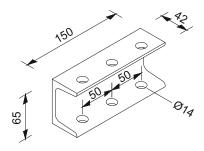


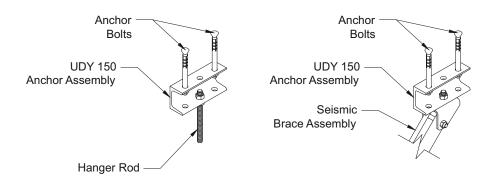
# **STEP 12**

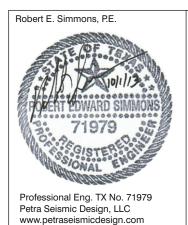
## **Determining Brace Anchor**

Where single anchor does not meet the design criteria, Use UDY 150 anchor assembly in order to increase anchor quantity. Group anchor calculations should be done in accordance with ACI 318 appendix D or by manufacturers approval other sources like ETAG. Consult with manufacturers design professional for more information.

#### UDY 150 Anchor Assembly:







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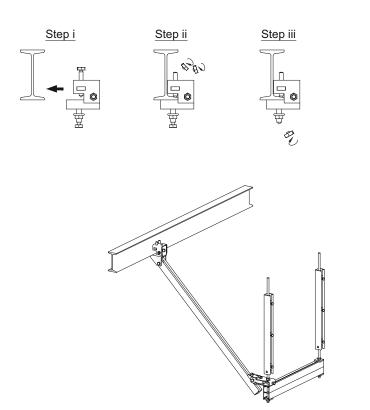


# **STEP 12**

## **Determining Brace Anchor**

In cases where fastening brace assembly to a steel beam, use EAE Steel Beam Fastener.

Installation Instructions for EAE Steel Beam Fastener:



#### Step i:

Place fastener assembly to steel beam's bottom flange.

#### Step ii

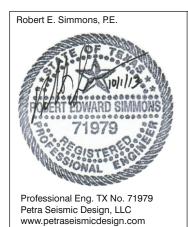
Fasten upper bolts until their heads breaks off.

#### Step iii :

Fasten bottom bolt until it's head breaks off.

#### Step iv

Fasten brace ceiling attachment to bottom bolt with nut (recommended torque 25 Nm).



Robert E. Simmons, PE, Petra Seismic Design, LLC has reviewed this drawing for compliance with the IBC and accepted engineering practice for non-structural seismic restraint components. Only the components are verified to meet published design strengths if installed per this manual. Users of this document assume all risk and liability. Restraint level, selection, location and layout must be approved by a seismic design professional. The registered design professionals for Mechanical, Electrical, Plumbing, Fire and Structural are responsible for their pertinent design scope. Structural engineer must approve loads applied to the structure. Drawings, and/or comments shall not be construed as directing the Contractor from complying with project plans and specifications, nor departures there from. Neither EAE, PSD, or Robert Simmons are the project design professionals.



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Date: 10/01/2013

Step iv



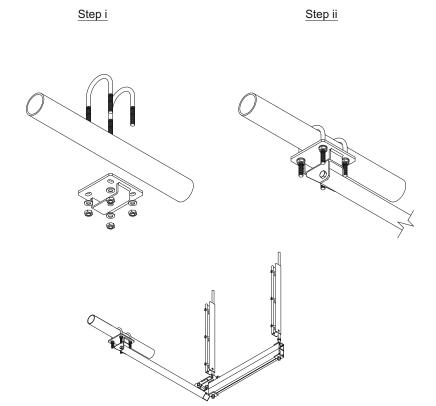


# **STEP 12**

## **Determining Brace Anchor**

In cases where fastening brace assembly to a pipe beam, use EAE Pipe Beam Fastener.

Installation Instructions for EAE Pipe Beam Fastener:

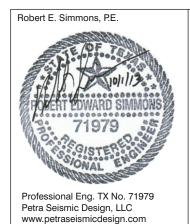


#### Step i:

Fasten U bolts to fastener plate with nuts and washers (recommended torques for M8 Nuts 15 Nm, M10 nuts 20 Nm, M12 nuts 25 Nm, M16 nuts 30 Nm)

#### Step ii

Fasten brace ceiling attachment to beam fastener with M12 bolt and nut (recommended torque 25 Nm)



Robert E. Simmons, PE, Petra Seismic Design, LLC has reviewed this drawing for compliance with the IBC and accepted engineering practice for non-structural seismic restraint components. Only the components are verified to meet published design strengths if installed per this manual. Users of this document assume all risk and liability. Restraint level, selection, location and layout must be approved by a seismic design professional. The registered design professionals for Mechanical, Electrical, Plumbing, Fire and Structural are responsible for their pertinent design scope. Structural engineer must approve loads applied to the structure. Drawings, and/or comments shall not be construed as directing the Contractor from complying with project plans and specifications, nor departures there from. Neither EAE, PSD, or Robert Simmons are the project design professionals.



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# STANDARDS & CERTIFICATES

#### >> SEISMIC STANDARDS & TEST CERTIFICATES

VIRLAB S.A. TEST LABORATORY - SPAIN

- ✓ IEEE 693-2005 » North American Standard
- ✓ EN 60068-3-3:1993 >> European Standard



# SEISMIC Qualification Certificate

Delivered on: Thursday, 26 September 2013

#### References:

- VIRLAB test procedure number 130612E2, issue 0, dated 12/06/2013: "Standard Test Procedure for Seismic Qualification of a Cable Tray Assembly from "EAE ELEKTROTEKNIK SAN VE TIC A.Ş." according to IEEE Standard 693-2005 and European Standard EN60068-3-3:1993".
- European standard EN 60968 3-3: 1993: Environmental testing Part 3: Guidance. Seismic test methods for equipments.
- North American standardEEE- 693/2005: "IEEE Recommended Practice for Seismic Design of Substations".
- European standard EN 60068 2-6: 2008: Environmental testing Part 2-6: Tests Fc: Vibration (sinusoidal).
- European standard EN 60068 2-47: 2005: "Environmental testing— Part 2-47: Tests. Mounting of specimens for vibration, impact and similar dynamic tests".

Laboratory Name:

**VIRLAB, S.A.** (accredited by ENAC, Spanish National Accreditation Entity). ENAC certificate number 54/LE131.

Laboratory Address:

Polígono Industrial de Asteasu, Zona B – 44 Apartado 247 20159 ASTEASU (SPAIN)

Equipment tested:

An "AN ASSEMBLY OF:UKS, UKF, CT Cable Trays, CR Cast resin Busbar, URC Trolley Busbar, KX Busbar, Wind Busbar Module AND AT3, AT4, AT5, UPD, STS, LP4, UDD, UDYB, UDY, IDD AND IDY HANGER ASSEMBLIES from EAE ELEKTRİKSAN VE TİC A.Ş", according to the set of drawings number TRF001, of EAE ELEKTRIK, dated 26/03/2013.

Photograph included here below shows the *Assembly* on the test platform.



#### REPORT ON THE SEISMIC QUALIFICATION TESTS OF

#### "AN ASSEMBLY OF:

UKS, UKF, CT Cable Trays, CR Cast resin Busbar, URC Trolley Busbar, KX Busbar, Wind Busbar Module AND AT3, AT4, AT5, UPD, STS, LP4, UDD, UDYB, UDY, IDD AND IDY HANGER ASSEMBLIES from EAE ELEKTRİKSAN VE TİC A.Ş",

ACCORDING TO IEE STANDARD 693-2005 AND EUROPEAN STANDARD EN 60068-3-3:1993

NOTE: As indicated in section 5.10.2 of Standard ISO-IEC 17025:2005, it is stated that:

The results of this report concern the simple tested solely and exclusively.

The Laboratory forbids the <u>partial</u> reproduction of this document without written authorisation.

Date Carried out by: Revised by:

VIRLAB, S.A.

Division of URBAR INGENIEROS, S.A.

Denis AGOTE

Juan Antonio PÉREZ Polígono Industrial of Asteasu Zona B, Pabellón 44 20159 ASTEASU (Gipuzkoa) SPAIN www.virlab.es E-mail: virlab@urbar.com Tel.: +34 943 69 15 00 Fax: +34 943 69 26 67



#### ▶▶6. Product Specifications



#### SEISMIC BRACING GENERAL PRODUCT SPECIFICATIONS FOR SUSPENDED DISTRIBUTION SYSTEM AND EQUIPMENTS (E-LINE SEISMIC)

#### **General Description:**

Technical precautions should be done for the suspended electrical&mechanical distribution systems and equipments in the building against suffering in case of earthquake occurrence. Distribution systems should not pose a threat to life and property security after an earthquake. Distribution systems and equipments in the building should be protected against earthquakes with seismic braces, which should be in accordance to the standards and technical specifications given below.

#### Standards & Certifications:

- Seismic bracing systems should be tested and certificated in an internationally accepted and accredited test laboratory according to IEEE 693 standard and EN 60068-2-6, EN 60068-2-47, EN 60068-3-3 norms
- Calculated according to IBC 2012 horizontal seismic acceleration, stated allowable loads of seismic braces should be approved by an IBC authorized seismic design engineer (P.E., Professional
- Seismic bracing systems should be in compliance with the schematic details in FEMA412,413,414.
- Seismic bracing systems should be manufactured in a facility, where ISO 9001 quality management and ISO 14001 environmental management procedures are being followed.

#### System General Composition:

Finishes of seismic brace systems should be hot-dip galvanized for rigid seismic brace section and alkali zinc coated for bolts/nuts, rod connection and other fastening components according to below stated composition. The bolt, which connects rigid brace section to distribution system, should be torque controlled or provided with a proper tool for this torque level.

#### 3.1- Mechanical Strength:

- Calculated according to AISI 1999 ASD, stated allowable compression loads for section length and thickness of rigid seismic brace sections should be approved by an IBC authorized seismic design engineer (P.E., Professional Engineer).

#### For 2.5mm Seismic Brace Section Thickness:

: 12.61 kN Allowable Compression Load 1.5 m : 9.20 kN Allowable Compression Load 3 m : 5.53 kN Allowable Compression Load

#### For 2mm seismic Brace Section Thickness:

: 8.43 kN Allowable Compression Load 1.5 m 2 m : 6.13 kN Allowable Compression Load : 3.83 kN Allowable Compression Load

#### 3.2- General Body Structure:

- Fastening piece, which connects brace to threaded rods, should be compatible to M8-M10-M12 or M14-M16-M20 rods and should be applicable to the installed hanger, without requiring rod hanger to be dismantled.
- Determined by threaded rod length and diameter, rod stiffeners should be applied.
- Calculated according to AISI 1999 ASD and IBC 2012 load combinations, stated trapeze hanger allowable loads on seismic brace applications should be approved by an IBC authorized seismic design engineer (P.E., Professional Engineer).
- Other than threaded rods, seismic braces should have compatible fastening accessory for the hanger, which braces are being attached.
   Seismic brace body should have rotational joints, which allows optimum 45 degrees installation angle in accordance with FEMA 412, 413, 414 along with various installation angles. Stated allowable horizontal seismic loads for variable installation angles should be approved by an IBC authorized seismic design engineer (P.E., Professional Engineer)
- Seismic brace should be compatible for lateral (transverse) and longitudinal brace connections.
- Brace length should be adjustable without requiring rigid brace section to be cut. Where needed, brace system should also allow rigid brace section to be cut.
- -Rigid brace section should be hot-dip galvanized approximately 55 µm in a facility, where galvanizing is available according to EN ISO 1461 standard.

   Bolts/nuts, rod connection and other pieces should be passivized and lacquered over alkali zinc according to DIN 50961 standard. Thickness of the coating should be between 7-12 µm and should be able to complete 400 hours of salt-spray test.

#### 3.3- Structural Connection:

- Loads of the anchor/bolt of the structural connection should be stated with prying factor. Stated loads should be approved by an IBC authorized seismic design engineer (P.E., Professional Engineer).
- The design of the structural connection component should be able to minimize the prying factor in 35-70 degrees of installation angle range.
- Seismic brace should have appropriate accessories for fixing to steel structures.

#### 3.4- Secure Head-off Bolt/Conic Bolt:

- Secure head-off bolt, which serves rigid brace section length adjustment, should be 8.8 steel or upon request A70 stainless steel.
- Conic bolt, which can be used instead of secure head-off bolt, should be 8.8 steel.

#### 3.5- Rod Stiffener:

- Rod stiffeners should be used only on the seismic brace connections, where threaded rod hangers of the distribution system exceed diameter and length stated below. Maximum spacing of rod stiffener pieces should also be stated and approved by an IBC authorized seismic design engineer (P.E., Professional Engineer). Maximum M8 rod length without stiffener : 300 mm

Maximum M10 rod length without stiffener: 475 mm Maximum M12 rod length without stiffener: 625 mm Maximum M16 rod length without stiffener: 775 mm Maximum M20 rod length without stiffener: 925 mm

#### Distribution System Connection:

- In compliance with FEMA 412,413,414, U bolts or special fixing pieces for the distribution system should be used on hanger sections, where hangers fastened with brace. The distribution system should not be left unrestrained.

#### Application & Installation:

- The suspended distribution systems should be restrained with transverse (lateral) and longitudinal seismic braces.
- -Spacing between two transverse (lateral) brace should not exceed, 12m for heating&cooling and plumbing pipes, stated values in NFPA for sprinkler pipes and stated values in SMACNA seismic restraint guidelines for HVAC ducts.
- Spacing between two transverse (lateral) brace should not exceed 9m for electrical busbars and cable trays, 12m for electrical conduit pipes.
- Spacing between two transverse (lateral) brace should not exceed 6m for the pipes, in which flows life endangering fluids, toxic or explosive in nature.
- Spacing between two longitudinal brace should not exceed two times the values stated above for related distribution system.
- Seismic bracing systems should be installed according to calculated strengths, product types and figures shown in these calculations. Installations instructions of the manufacturer should be followed carefully. Secure head-off bolts should be fastened until its head breaks off and then fixed with nuts. Conic bolts should be fastened with proper tools for stated torque levels and then fixed with nuts.
- After the installation, heads of the secure bolts should be checked to approve that installation is done with appropriate torque levels.







# **ELINESEISMIC**





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# **PRODUCT TYPES**



#### **BUSBAR ENERGY DISTRIBUTION SYSTEMS**

**CABLE TRAYS** 





TROLLEY BUSBAR ENERGY DISTRIBUTION SYSTEMS



**INDOOR SOLUTIONS** 



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#### EAE Elektrik A.Ş.

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